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4 H- parameters 5. Inverse H- parameters/9-parameters.

1. 7- parameters / open circuit parameters. 2. 4- parameters / short circuit parameters 3. ABCD - parameters / Transmission parameters

11 TOO port network parameters are classified into

ports and is' no of input not.

suppose we taken - n port network has 'n' no. q output

port is having one receiving end and one sending end. 700 port means two sending ends and 7000 receiving ends.

1.700-port networks

2

Equivalent circuit:  
for equation (1) 
$$f(z)$$
  
  
 $f(z) = \int_{1}^{1} \frac{1}{2u} \int_{1}^{1} \frac{1$ 

from eqn(1) 
$$\mathcal{L}(\mathbf{x})$$
  

$$J_{1:} Y_{11} \cup U_{1} + Y_{12}(\mathbf{x})$$

$$\boxed{Y_{11} = \frac{g_{1}}{U_{1}} \cup U_{2:\tau 0}}$$
and  $J_{2:} Y_{21} \cup U_{1} + Y_{22}(\mathbf{x})$   

$$\boxed{Y_{21} = \frac{J_{2}}{U_{1}} \cup U_{2:\tau 0}}$$
if  $U_{1:0}$ ; the part-1 is short circuit  
 $U_{1:0}$   $\boxed{U_{1}} \cup U_{2:\tau 0}$   
from eqn(1)  $\mathcal{L}(2)$   
 $J_{1:} Y_{11}(\mathbf{x}) + Y_{12} \cup U_{2}$   

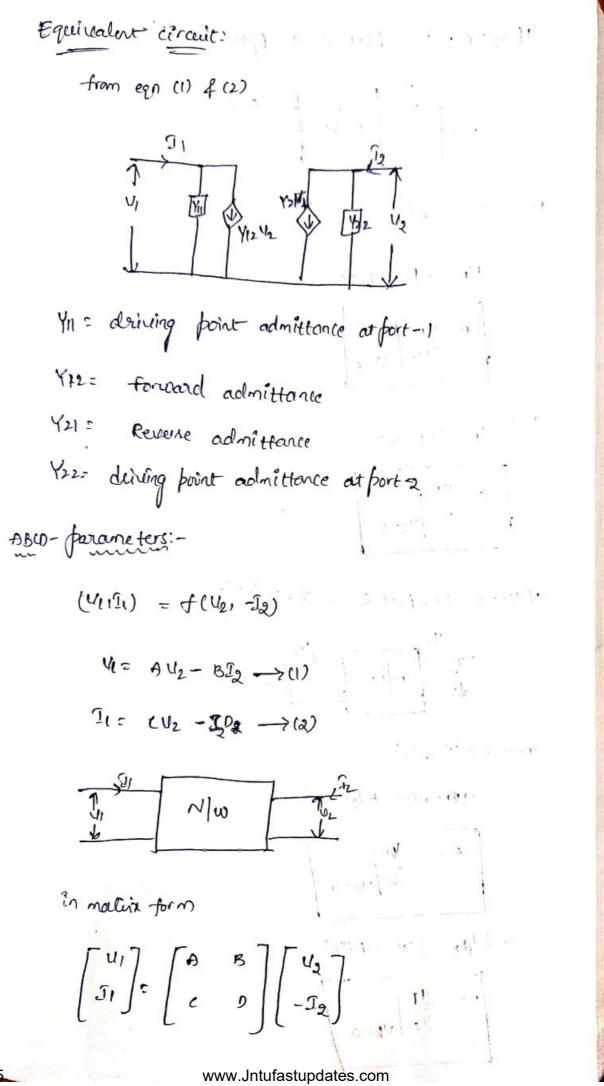
$$\boxed{Y_{12} = \frac{J_{1}}{U_{2}} \cup U_{1:\tau 0}}$$
and  $J_{2:} = Y_{21}(\mathbf{x}) + Y_{22} \cup U_{2}$   

$$\boxed{Y_{22:} = \frac{J_{2}}{U_{2}} \cup U_{1:\tau 0}}$$
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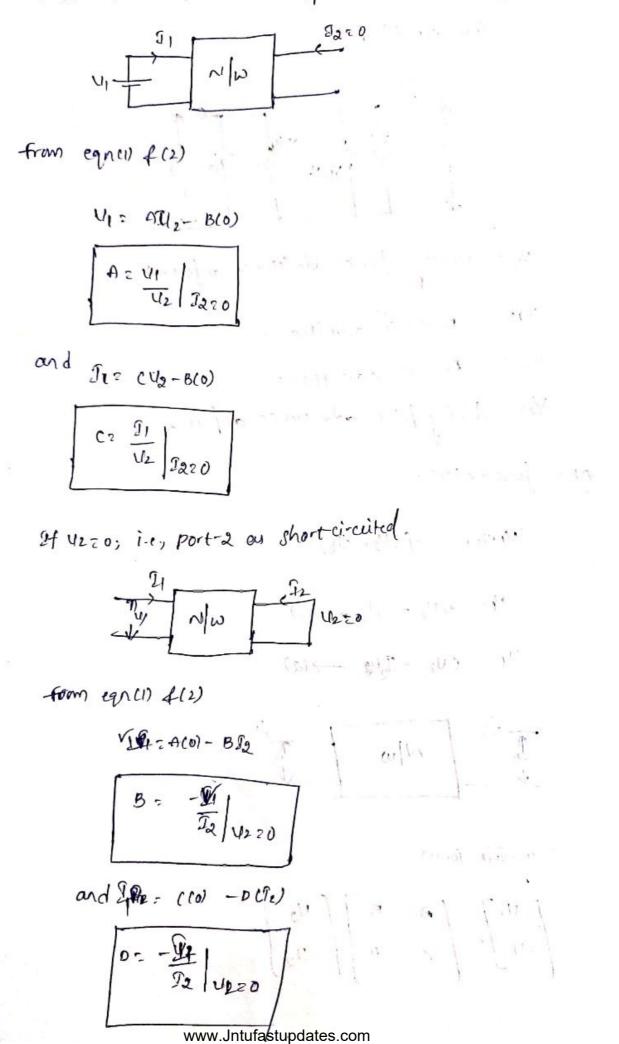
4

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L



Of J2=0; i.e., port-2 as open circuit



$$I_{\text{trivialist}} \quad \text{trivialist} \quad \text{trivia$$

and  

$$Jz: h_{21} I_{1} + h_{22}(z)$$

$$h_{21} := \frac{J_{2}}{J_{R}} |_{U_{27}} z$$

$$J = \int \frac{J_{2}}{J_{R}} |_{U_{27}} z$$

$$J = \int \frac{J_{2}}{J_{12}} |_{U_{27}} z$$

$$J_{12} := \int \frac{J_{12}}{J_{12}} |_{U_{27}} z$$

$$J_{12} := \int \frac{J_{12}}{J_{12}} |_{U_{27}} z$$

$$J_{12} := \int \frac{J_{21}}{J_{12}} |_{U_{27}} z$$

$$h_{11} \Rightarrow fon coard in pedence$$

$$h_{22} \Rightarrow fon coard vottage pain$$

$$h_{21} \Rightarrow Revenu current gain.$$

$$h_{22} \Rightarrow backwoord in pedence$$

8

$$\begin{aligned} & \mathcal{R}elabions: \\ & \mathcal{R}eparameters is terms of  $\mathcal{Y} - parameters: \\ & \mathcal{I} = \frac{1}{\mathcal{Y}} = \mathcal{I}\mathcal{Y}\mathcal{J}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{Y}\mathcal{H} & \mathcal{Y}\mathcal{L}_{2} \\ \mathcal{Y}\mathcal{L}\mathcal{I} & \mathcal{Y}\mathcal{L}_{2} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{Y}\mathcal{H} & \mathcal{Y}\mathcal{L}_{2} \\ \mathcal{Y}\mathcal{L}\mathcal{I} & \mathcal{Y}\mathcal{L}_{2} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{Y}\mathcal{L} & \mathcal{Y}\mathcal{L} \\ \mathcal{Y}\mathcal{L}\mathcal{I} & \mathcal{Y}\mathcal{L}_{2} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{Y}\mathcal{L} & -\mathcal{Y}\mathcal{H}\mathcal{L} \\ -\mathcal{Y}\mathcal{L}\mathcal{I} & \mathcal{Y}\mathcal{H} \end{bmatrix} \\ \begin{bmatrix} \mathcal{R}\mathcal{L} & \mathcal{R}\mathcal{R} \\ \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{L} & -\mathcal{Y}\mathcal{I}\mathcal{L} \\ -\mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{L} & -\mathcal{Y}\mathcal{I}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{L} & -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{L} & -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{L} & -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{L} & -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{R}\mathcal{I} & -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} & -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix}^{-1} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix} \\ & \cdot \begin{bmatrix} \mathcal{R}\mathcal{I} & \mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \\ -\mathcal{R}\mathcal{I} \end{bmatrix} \\ & \cdot \begin{bmatrix} \mathcal{$$$

\_ 9

H2-parameters is terms of ABCD- Parameters.

we know that 2-parameters equations

and ABCD- parameters ,

$$V_{1}: AV_{2} - BR_{2} \longrightarrow (3)$$

$$S_{4}: (V_{2} - DV_{2} \longrightarrow (4))$$

$$(4) \implies CU_{2}: S_{1} + D\tilde{I}_{2}$$

 $V_{2} = \frac{1}{C}I_{1} + \frac{2}{C}I_{2} \rightarrow (5)$ substitulte (5) in (3)

$$U_{1} = \Theta \left[ \frac{1}{c} \widehat{I}_{1} + \frac{1}{c} \widehat{I}_{2} \right] - B \widehat{I}_{2}$$

$$= \frac{1}{c} \widehat{I}_{1} - \left( B \underbrace{-}_{c} \widehat{P}_{1} \right) \widehat{I}_{2} \longrightarrow (c)$$

compain q (1) & (6) Equations

$$z_{11} = A_{12}$$
,  $z_{12} = \begin{bmatrix} -B(+AD) \\ -C \end{bmatrix}$ 

Comparing (2) & (5) Equations

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$$\begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} +-parameters \\ \text{wetrow that } 2-parameters equations \\ \\ \begin{array}{l} \text{wetrow that } 2-parameters equations \\ \\ \\ \text{Wetrational form } \\ \\ \begin{array}{l} \text{Wetrational form } \\ \\ \begin{array}{l} \text{Wetrational form } \\ \\ \begin{array}{l} \text{Wetrational form } \\ \\ \text{Wetrational form } \\ \\ \end{array} \end{array}$$

$$\begin{array}{l} \begin{array}{l} \text{Wetrational form } \\ \\ \text{Wetrational form } \\ \\ \begin{array}{l} \text{Wetrational form } \\ \\ \begin{array}{l} \text{Wetrational form } \\ \\ \end{array} \end{array}$$

$$\begin{array}{l} \text{Wetrational form } \\ \\ \begin{array}{l} \text{Wetrational form } \\ \\ \mbox{Wetrational form } \\ \\ \mbox{Wetrational form } \\ \end{array} \end{array}$$

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\* Uparameters is terms of 2-parameters:  
y parameters equations are  
It: Yn Up + Up V\_2 ->00  

$$f_2 = Y_{21} U(1 + Y_{12} V_2 ->02)$$
  
 $Y = \frac{1}{t} = (t_1)^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2z_2 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$   
 $= \begin{bmatrix} 2n & 2t_1 2 \\ 2p & 2t_1 2 \\ 2p & 2t_1 \end{bmatrix}^{-1}$ 

12

y 4 parameters in terms of arean-faranutm.  
4 parameter 
$$I_1 = 411 U_1 + 4_{12} V_2 \rightarrow (1)$$
  
 $S_2 = 401 U_1 + 4_{22} V_2 \rightarrow (2)$   
ABOD-parameter equationly:  
 $U_1: AU_2 - E_{12} \rightarrow (3)$   
 $T = CU_2 - D_{12} \rightarrow (3)$   
 $T = CU_2 - D_{12} \rightarrow (3)$   
 $U_3 \Rightarrow B_{12} = AU_2 - U_1$   
 $I_2 = A U_2 - U_1$   
 $I_2 = A U_2 - U_1$   
 $I_2 = CU_2 - D \left[\frac{A}{B}U_1 \rightarrow (5)\right]$   
 $J_1 = \left[\frac{BC-AD}{B}\right]U_2 + \frac{O}{B}U_1 \rightarrow (6)^2$   
Compare  $C_1 E_1(6)$  equations  
 $Y_{11} = \frac{D}{B}$ .  $Y_{12} = \frac{BC-AD}{B}$   
Compare (2)  $E_1(6)$  equations  
 $Y_{21} = -Y_B$ ;  $Y_{12} = \frac{M(A)}{B}$ 

\* 4- parameters interms of hiparameters  
4+ Parameters Equation's are  
91: 411 414 412 42 ->102  
92: 421 414 412 42 ->102  
92: 421 414 412 42 ->102  
92: 421 414 412 42 ->102  
92: 421 414 412 42 ->102  
92: 421 414 412 42 ->102  
92: 421 414 412 42 ->103  
93: 421 412 42 ->103  
(3) => 41191: 41 - 412 42 ->105  
(4) => 92: 42: 
$$\left[\frac{1}{h_{11}} \cdot 42 - \frac{h_{12}}{h_{11}} \cdot 42\right] + h_{22} \cdot 42$$
  
 $= \frac{h_{21}}{h_{11}} \cdot 41 + \frac{h_{11}h_{22}}{h_{11}} \cdot 42 ->105$   
(4) => 92:  $h_{21} \left[\frac{1}{h_{11}} \cdot 41 + \frac{h_{11}h_{22}}{h_{11}} \cdot 42 ->105$   
(4) => 92:  $h_{21} \left[\frac{1}{h_{11}} \cdot 41 + \frac{h_{11}h_{22}}{h_{11}} \cdot 42 ->105$   
(4) => 92:  $h_{21} \left[\frac{1}{h_{11}} \cdot 41 + \frac{h_{11}h_{22}}{h_{11}} \cdot 42 ->105$   
(4) =>  $h_{21} = \frac{h_{21}}{h_{11}} \cdot 41 + \frac{h_{11}h_{22}}{h_{11}} + \frac{h_{22}}{h_{11}} \cdot 42 ->105$   
(4) =>  $h_{21} = \frac{h_{21}}{h_{11}} \cdot 41 + \frac{h_{11}h_{22}}{h_{11}} + \frac{h_{22}}{h_{11}} + \frac{h_{22}}{h_{11}} + \frac{h_{23}}{h_{11}} + \frac{h_{23}}{h_{12}} + \frac{h_{23}}{h_{11}} + \frac{h_{23}}{h_$ 

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1) ABOP for annelers in terms of 2-for an etwices  
ABOP for annelers Equations are:  
UIT A U2 - BJ2 -> (2)  
DIT (U2 - DJ2 -> (2)  
PIT 2001 + 2102 -> (2)  
(2) => 22001 + 2122 J2  
DIT = 
$$\frac{1}{221}$$
 U2 -  $\frac{222}{221}$  J2 -> (5)  
(3) => U12 211  $\left[\frac{1}{221}$ , U2 -  $\frac{222}{221}$  J2 -> (5)  
(3) => U12 211  $\left[\frac{1}{221}$ , U2 +  $\frac{212}{221}$  J2 -> (6)  
(a) =  $\frac{211}{221}$  U2 +  $\frac{212}{221}$  J2 -> (6)  
(a) for base (1) Q(6) equations  
PIT =  $\frac{211}{221}$  ; BT =  $\frac{21222}{221}$   
(compare (2))Q(5) equations  
C2  $\frac{2211}{221}$  ; DT =  $\frac{222}{221}$ 

XABOD parameters in terms of 4-parameters:-ABOD parameters Equations: U1: A 12- BJ2 -7(1)  $\mathfrak{G}(\mathfrak{c} (\mathcal{U}_{2} - \mathfrak{b}\mathfrak{I}_{2} \longrightarrow \mathfrak{b}) \qquad \mathfrak{s}(\mathfrak{c}) \qquad \mathfrak{s}(\mathfrak{c})$ 4- parameters Equations: $g_1: Y_{11} U_1 + Y_{12} U_2 \rightarrow (3)$ ?2= Y21 41+ Y22 42 →(4) (a) => 42141= J2- 42242 . · · · · · 41= 9 1 22 - 422 42 -2(5) 421 421 13) => 411 [ +21 22 - 422 42] +412 42  $21 = \frac{44}{42} 22 + 412421 - 411422 = ->(6)$ Yai mitro participarti compare (1) & (5) equations  $A = \frac{1}{421}$ ;  $B = \frac{422}{421}$ . compare (2) & (6) equations 12 412 421 - 411 422 ; D= - 411 421

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1

$$J B (0) for anishes in terms of h for anishes ?-$$

$$D (0) for anishes Equations:$$

$$U_{1} \in A U_{2} - BJ_{2} \rightarrow (1)$$

$$J_{1} \in C U_{2} - DJ_{2} \rightarrow (2)$$

$$H parameters Equations$$

$$U_{1} \in hu \partial u_{1} + h_{2} dJ_{2} \rightarrow (3)$$

$$J_{2} \leq h_{2} I \int u_{1} + h_{2} dJ_{2} \rightarrow (4)$$

$$(U) \Rightarrow h_{2} U_{1} \in J_{2} + h_{2} U_{2}$$

$$J_{1} \leq \frac{1}{h_{2}} J_{2} \neq \frac{h_{2} 2}{h_{2}} U_{2} \rightarrow (5)$$

$$(J) \Rightarrow U_{1} \leq hu \left[ \frac{1}{h_{2}} J_{2} \neq \frac{h_{2} 2}{h_{2}} U_{2} \rightarrow (5) \right]$$

$$U_{1} = hu \left[ \frac{1}{h_{2}} J_{2} \neq \frac{h_{2} 2}{h_{2}} + \frac{h_{2} 2}{h_{2}} \right] U_{2} \rightarrow (2)$$

$$Coultar (U) g_{1}(s) equations$$

$$A = \left[ \frac{hu h_{2} 2 + h_{2} h_{2}}{h_{2}} \right] ; B_{2} - \frac{h_{2}}{h_{2}}$$

$$Coultar (2) f(6) equations$$

$$c_{2} - \frac{h_{2}}{h_{2}} ; D_{2} = \frac{1}{h_{2}}$$

J h-farameters in terms 
$$d_1 \neq -farameters$$
  
h-farameter Equations are:  
 $V_{12} = h_{11} + h_{12} V_2 \rightarrow (1)$   
 $g_1 = h_{11} g_{11} + h_{12} V_2 \rightarrow (1)$   
 $g_2 = h_{12} g_{11} + h_{22} V_2 \rightarrow (2)$   
 $g_2 = h_{12} g_{11} + g_{22} g_{22} \rightarrow (2)$   
 $V_2 = g_2 g_{11} + g_{22} g_{22} \rightarrow (2)$   
 $V_2 = g_2 g_{11} + g_{22} g_{22} \rightarrow (2)$   
 $V_2 = g_2 g_{11} + g_{22} g_{22} - g_{22} g_{11}$   
 $V_2 = g_2 g_{12} + V_2 - g_{22} g_{11}$   
 $V_2 = g_{11} g_{12} + g_{22} g_{12} - g_{12} g_{11}$   
 $V_1 = g_1 g_2 - g_2 g_{22} - g_2 g_{11} - g_2 g_{11}$   
 $V_1 = g_1 g_2 - g_2 g_{22} g_{11} - g_{12} g_{11} - g_{12} g_{11}$   
 $V_1 = g_1 g_2 - g_2 g_{22} g_{11} - g_{12} g_{12} - g_{12} g_{11} - g_{12} g_{11} - g_{12} g_{12} - g_{12} g_{11} - g_{12} g_{12} - g_{12} g_{12} g_{11} - g_{12} g_{12} g_{12} g_{12} - g_{12} g_{12}$ 

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and a second

e h parameters in terms of 
$$y - parameters$$
:  
h parameter equations are:  
 $u_{12} = h_{11} J_{11} + h_{22} v_{2} \rightarrow (2)$ .  
 $y_{2} = h_{21} J_{11} + h_{22} v_{2} \rightarrow (2)$ .  
 $y_{-} parameter Equations$ :  
 $J_{12} = y_{11} v_{11} + y_{12} v_{2} - 7(3)$   
 $y_{2} = y_{21} v_{11} + y_{22} v_{2} - 7(3)$   
 $y_{2} = y_{21} v_{11} + y_{22} v_{2} - 7(3)$   
 $(u) \Rightarrow J_{2} = y_{21} \left[ \frac{1}{y_{11}} J_{1} - \frac{y_{12}}{y_{11}} v_{2} \right] + y_{22} v_{2} - 7(6)$   
 $compare (1) f (5) equations$   
 $h_{112} = \frac{y_{21}}{y_{11}} , h_{12} = \frac{-y_{12}}{y_{11}} ,$   
 $compare (a) f (6) equations$   
 $h_{21} = \frac{y_{21}}{y_{11}} , h_{22} = \frac{y_{11} y_{22} - y_{12} y_{21}}{y_{11}}$ 

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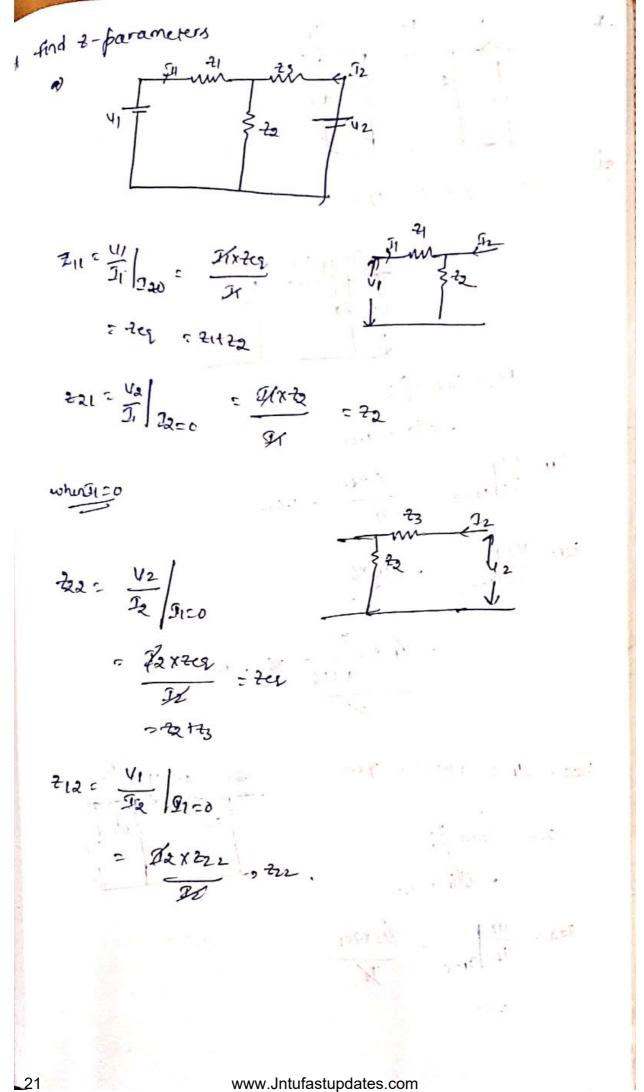
-

h parameters in terms of ABCO parameters  
h parameters acquations are:  

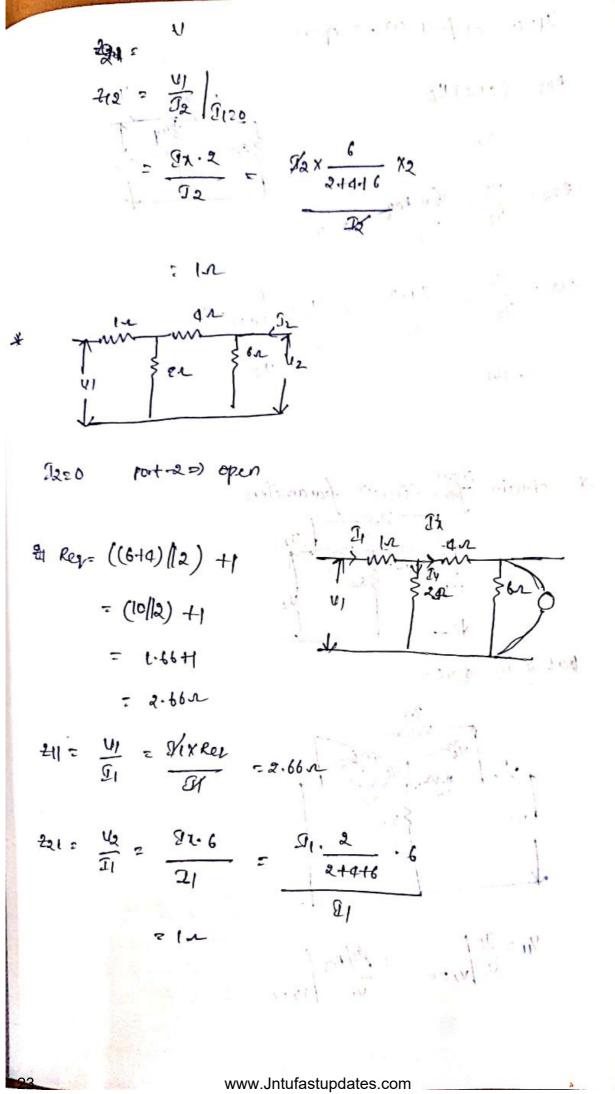
$$U_1 = h_{11}J_1 + h_{12}U_2 \rightarrow (a)$$
  
 $R_2 = h_{21}(I_1 + h_{22}U_2 \rightarrow (a))$   
 $R_{5CO}$  parameters equations are:  
 $U_1 = Ay_2 - BO_2 \rightarrow (3)$   
 $J_1 = (U_2 - DJ_2 \rightarrow (4))$   
 $(4) \Rightarrow OJ_2 = (U_2 - J_1)$   
 $J_2 = \frac{-}{D}U_2 - \frac{-}{D}J_1 \rightarrow (5)$   
 $(3) \Rightarrow U_1 = AU_2 - B \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $U_1 = \frac{AU_2 - B}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $U_1 = \frac{AU_2 - B}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $U_1 = \frac{AU_2 - B}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $L_1 = \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $L_1 = \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $L_1 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $L_2 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_3 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right]$   
 $L_4 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}U_2 - \frac{-}{D}E_1 \right] \right]$   
 $L_5 = \frac{-}{D} \left[ \frac{-}{D} \left[ \frac{-}{D}U_2 - \frac{-}{D}U_2 -$ 

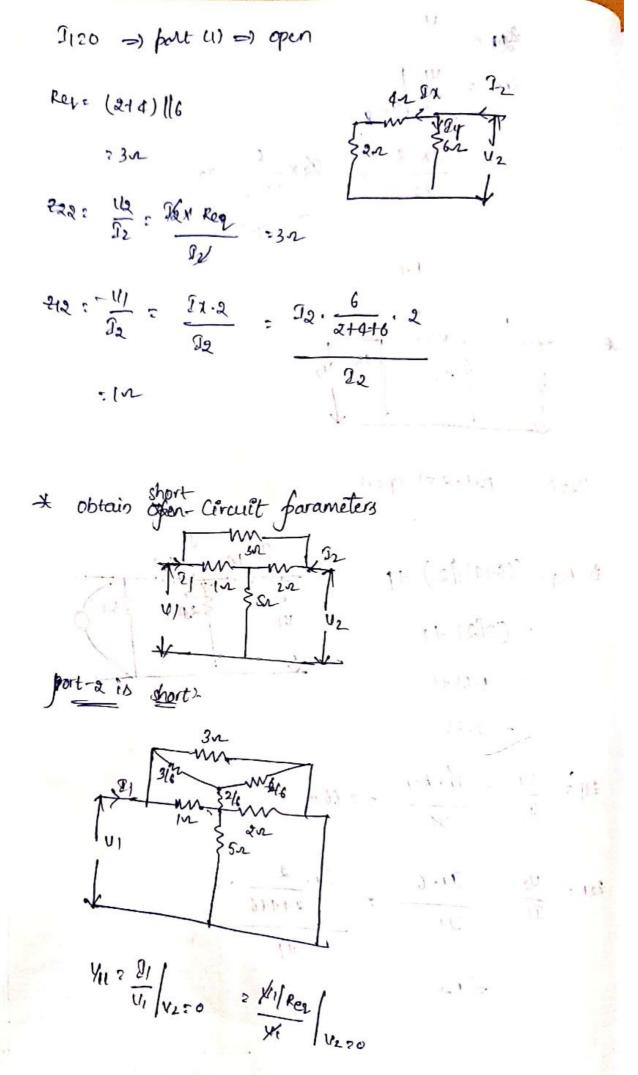
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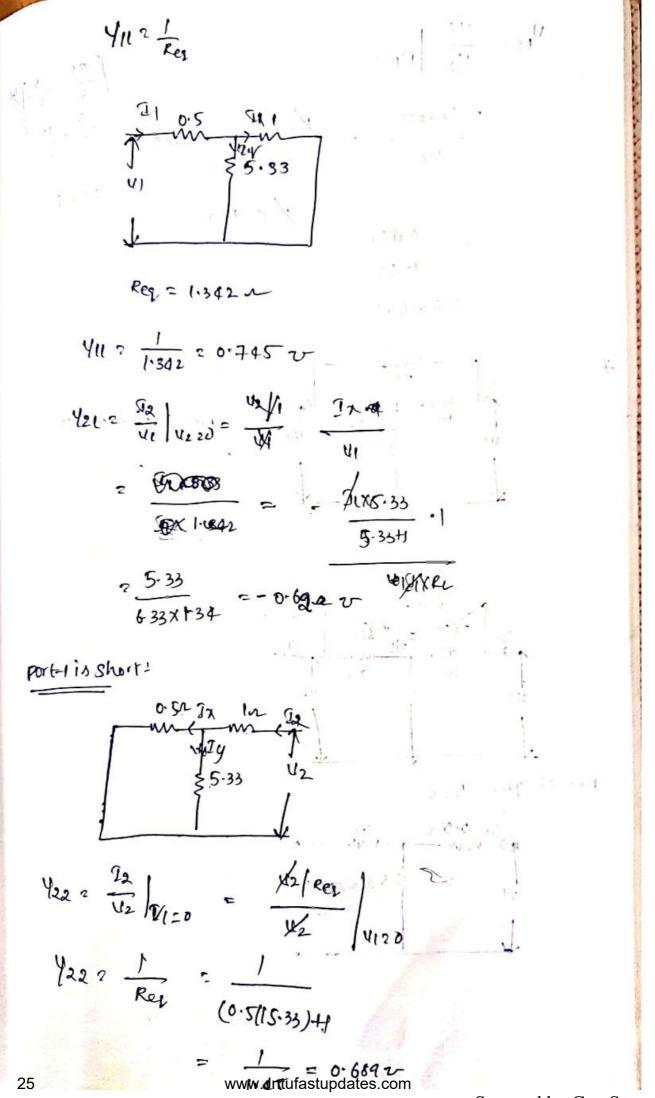
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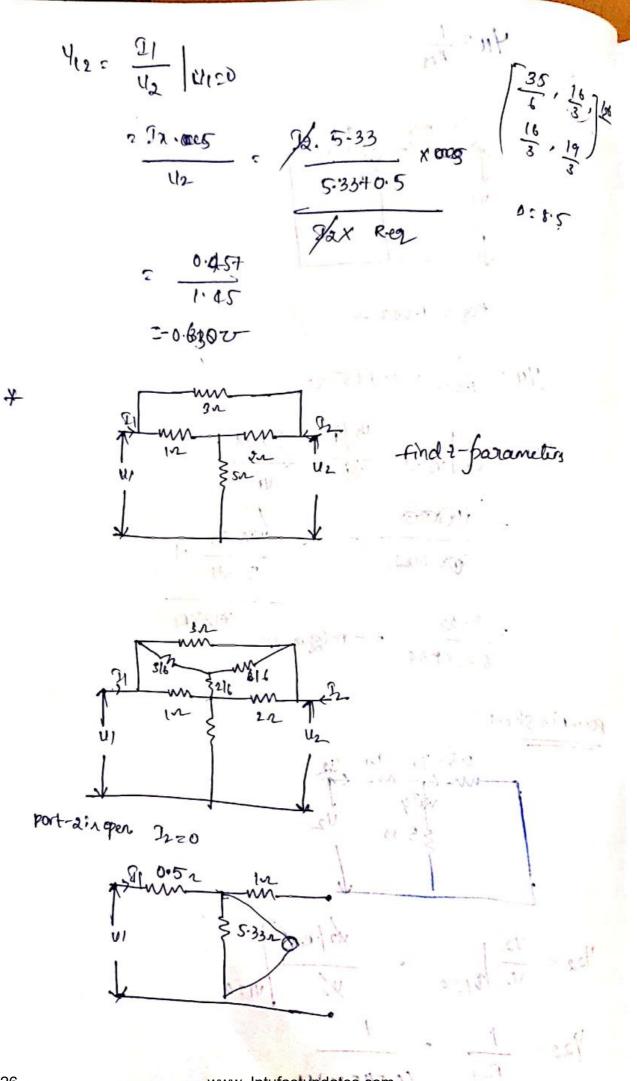


$$\frac{1}{2} \qquad \frac{1}{2} \qquad \frac{1}$$









$$keq = 0.5 + 6.33$$

$$= 5.33$$

$$2\pi = \frac{4\pi}{21} \int_{2\pi} \frac{2\pi}{21} \frac{4\pi}{21} = 5.833$$

$$\frac{2}{22} \left[ 2 \frac{4\pi}{21} \right]_{2\pi} \frac{\pi}{21} \frac{4\pi}{21} \cdot 533$$

$$= \frac{4(.533)}{31} = 5.333.4$$

$$port - 1 io Open Q_{1-0}$$

$$\frac{4\pi}{22} \cdot \frac{4\pi}{22} = Req = (+5.33)$$

$$\frac{7}{28} = Req = (+5.33)$$

$$\frac{7}{28} = \frac{4\pi}{21} \int_{2\pi} \frac{2\pi}{22} \cdot \frac{7}{24} = \frac{7}{28} \cdot \frac{2}{32} \cdot \frac{1}{32} \int_{3\pi} \frac{\pi}{26} \cdot \frac{533.4}{32}$$

$$\frac{2\pi}{28} = \frac{4\pi}{28} - \frac{4\pi}{38} \cdot \frac{2}{32} \cdot \frac{1}{32} = 5.33.4$$

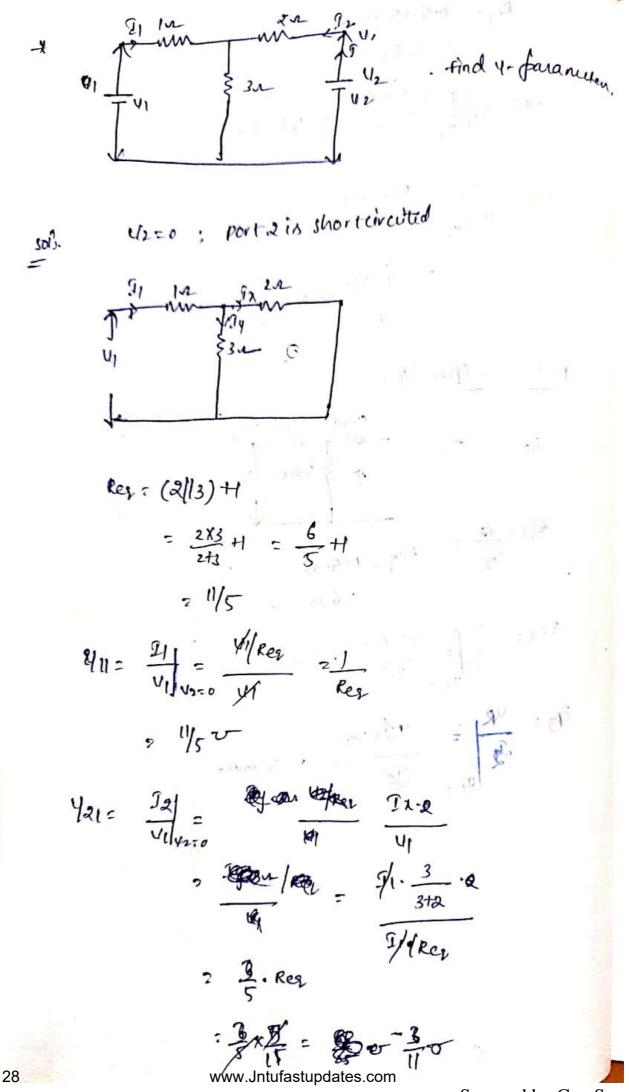
$$\frac{2\pi}{38} = \frac{4\pi}{38} - \frac{4\pi}{38} \cdot \frac{533}{34} = 5.33.4$$

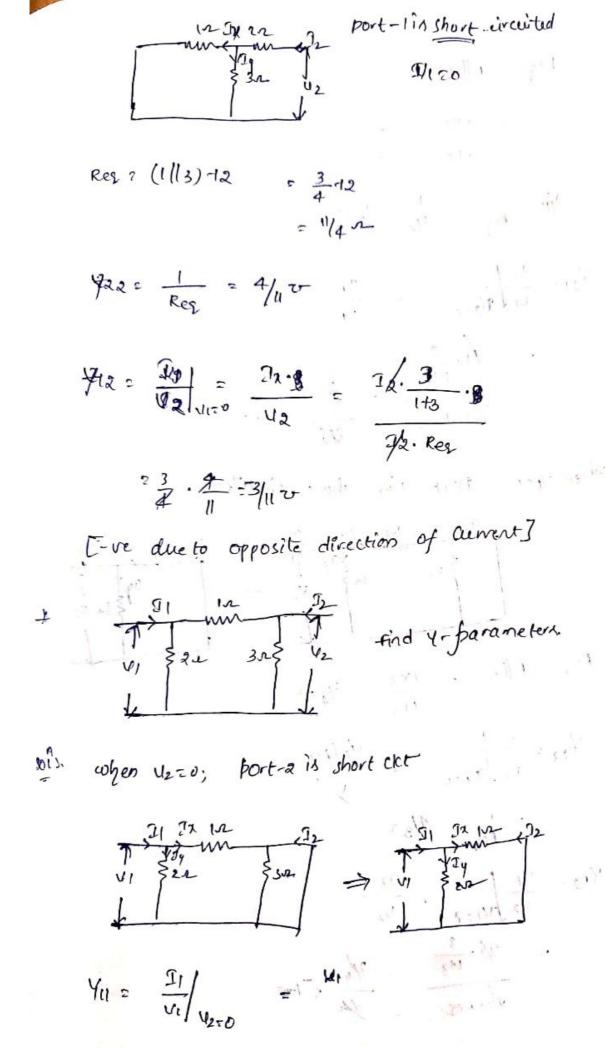
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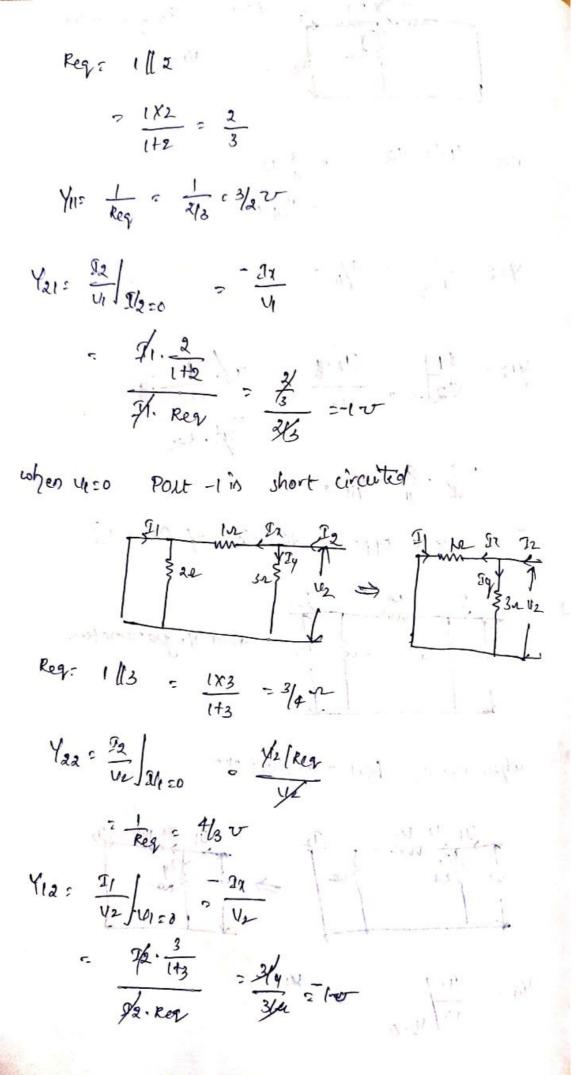
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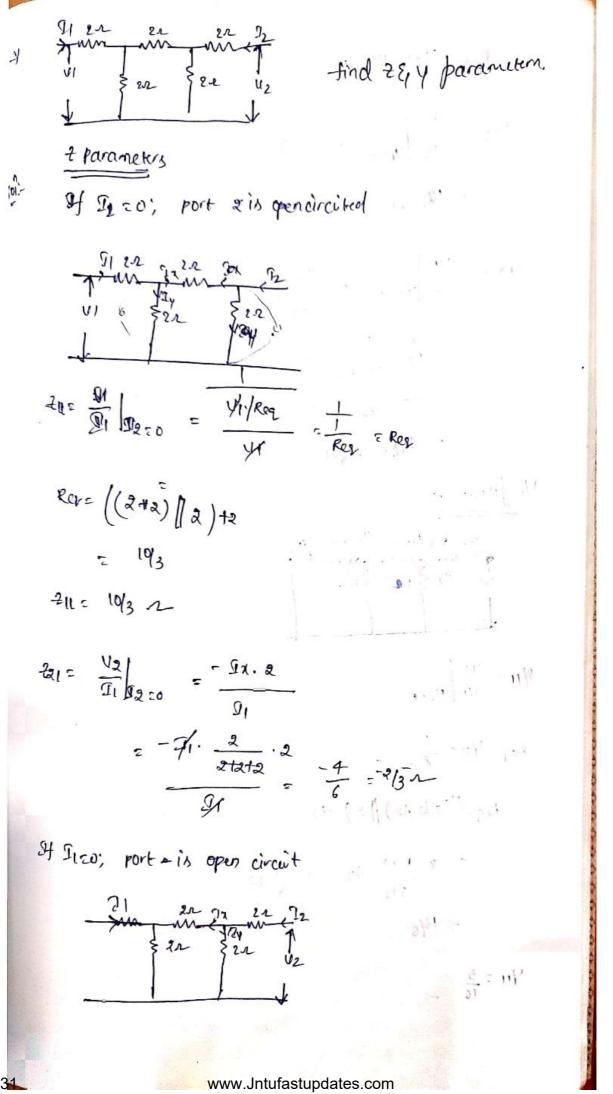


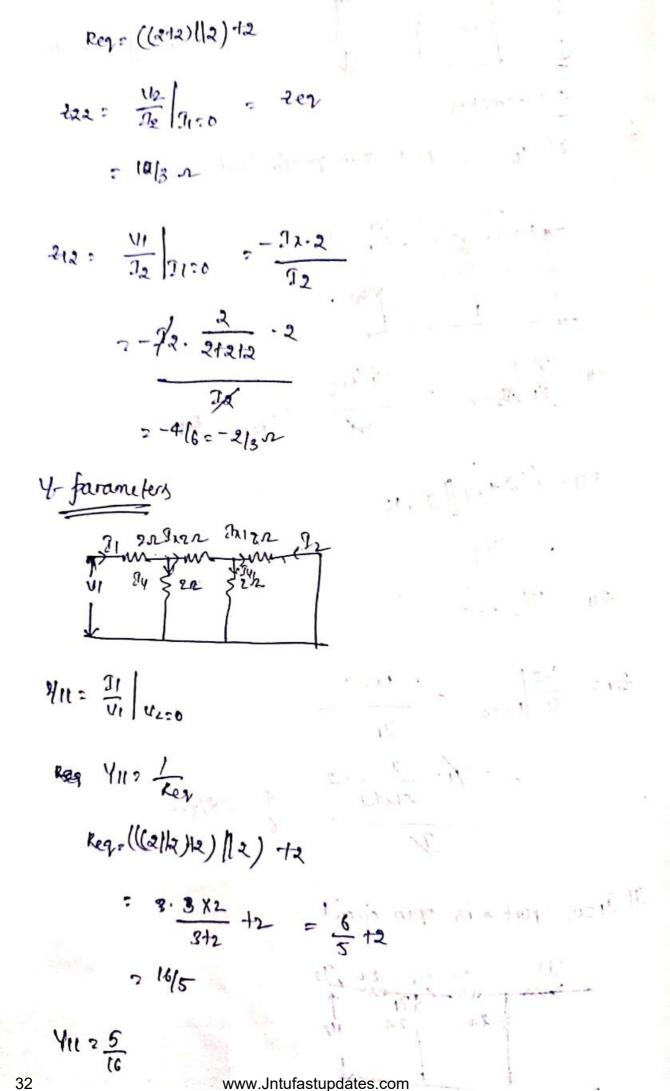




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$$Wa = \frac{\partial x}{\partial t} = \frac{\partial y}{\partial t} + \frac{\partial y}{\partial t}$$

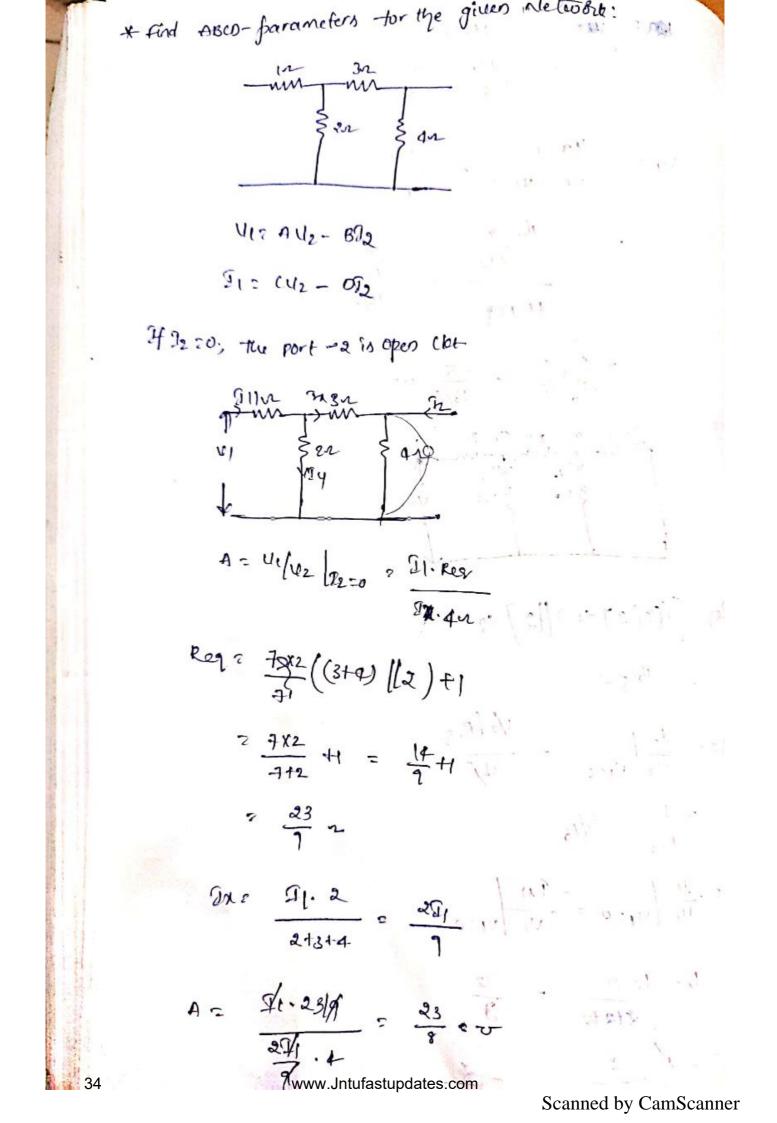
$$= \frac{2\eta}{6} = \frac{\eta}{3}$$

$$Y_{21} = \frac{q}{U_{1}} \Big|_{U_{1}\tau,0} = \frac{\eta}{U_{1}}$$

$$= -\frac{3!}{2t2} = -\frac{2}{(12)} + \frac{\eta}{U_{1}}$$

$$= -\frac{3!}{2t2} \times \frac{5}{16} = -\frac{5}{1656} - \frac{1}{1615} + \frac{\eta}{1615}$$

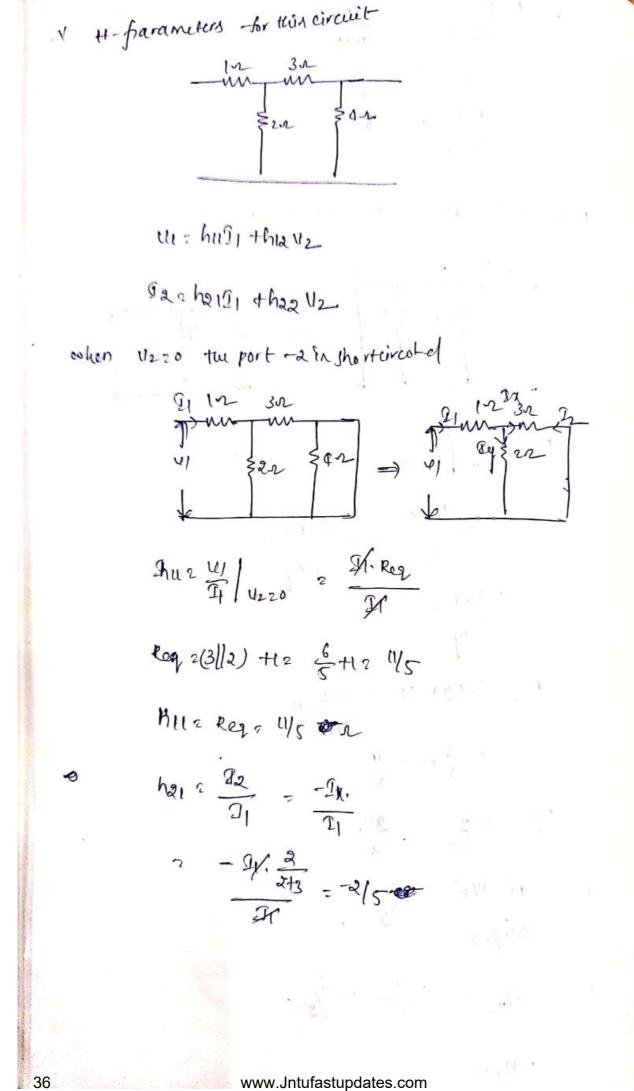
$$= \frac{1}{1615} \times \frac{1}{1615} + \frac{1$$



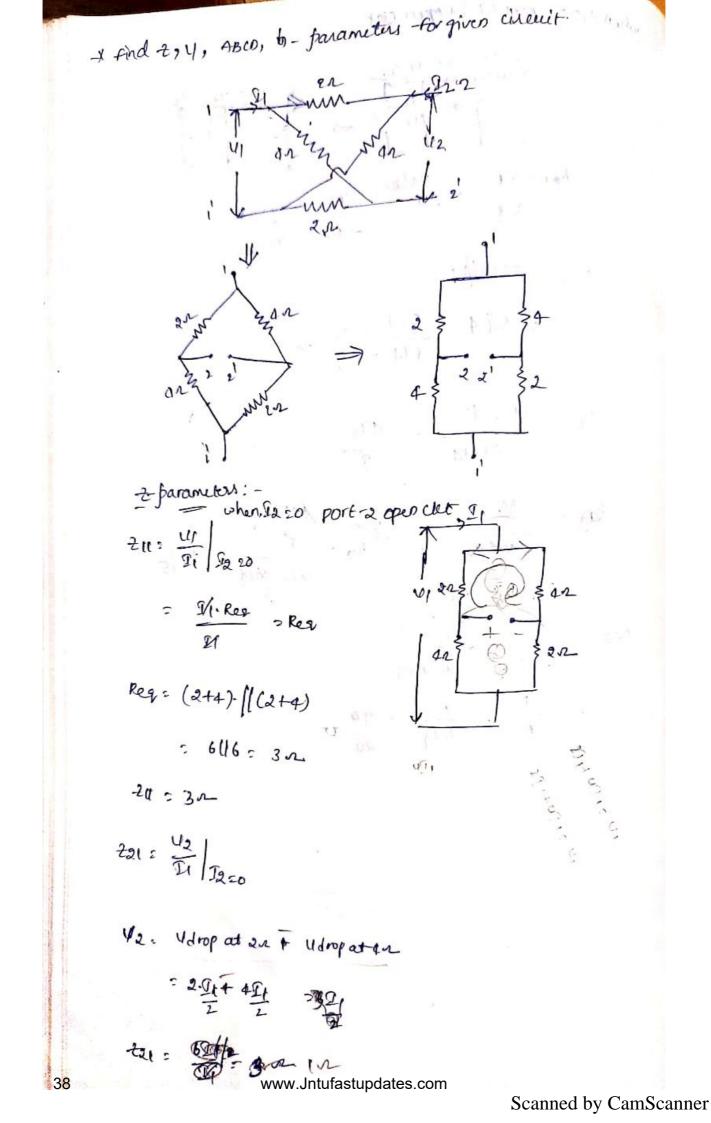
$$C=\frac{1}{\sqrt{2}}\int_{2}^{2}\frac{1}{\sqrt{2}}=\frac{1}{\sqrt{2}}\int_{1}^{2}\frac{1}{\sqrt{2}}=\frac{1}{\sqrt{2}}\int_{1}^{2}\frac{1}{\sqrt{2}}=\frac{1}{\sqrt{2}}\int_{1}^{2}\frac{1}{\sqrt{2}}$$

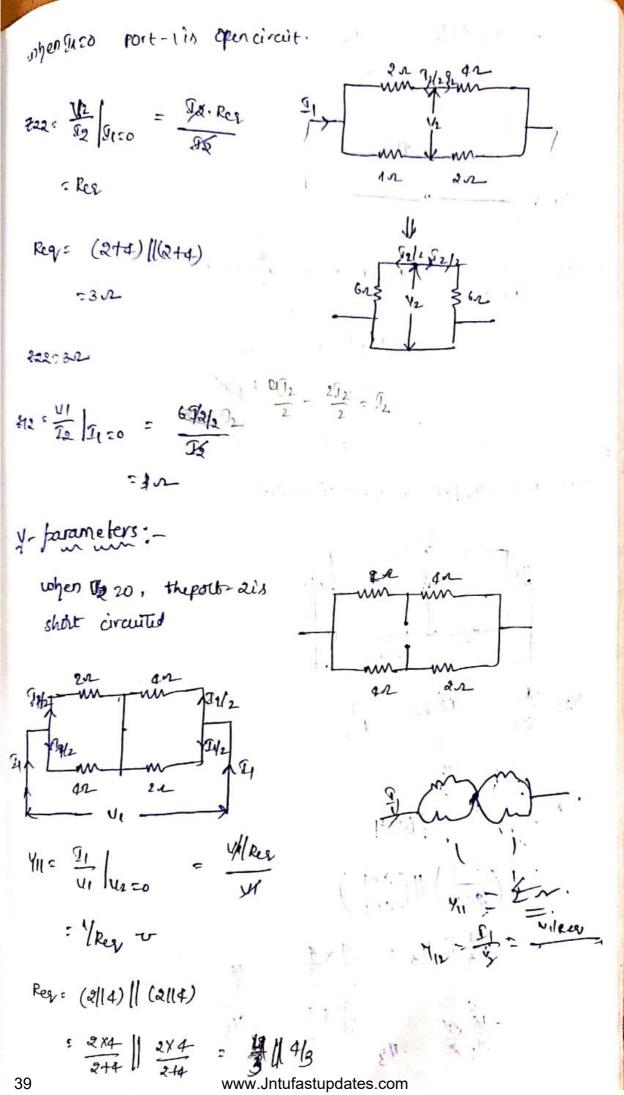
11 1 a mar 1 11

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when gizo portel inopen clet harze Viz = dadate 202 Iy.2 VIZ = -Ey Iz. Rev Reg = (2+3)/14 = 511 4 = 5×4 = 20 -5 8y = 12.4 = 412 $2t_{3}t_{4} = 412$ ha = - 4 the = - 4 the - 2/5 + 2/5 + 2/5 + 2/5 haa: Ja . 1/2 Uz Spirer  $= \frac{1}{keq} = \frac{1}{20|q} = \frac{q}{20} \tau$ 19 -1 SV. strepant. The stars is after a second 37 www.Jntufastupdates.com





$$= \frac{4}{4} \frac{x}{4} \frac{x}{4} \frac{1}{3} = \frac{16}{3}$$

$$= \frac{1}{4} \frac{1}{3} \frac{x}{4} \frac{1}{3} = \frac{1}{3}$$

$$= \frac{1}{4} \frac{1}{5} \frac{x}{4} \frac{1}{3} = \frac{1}{3}$$

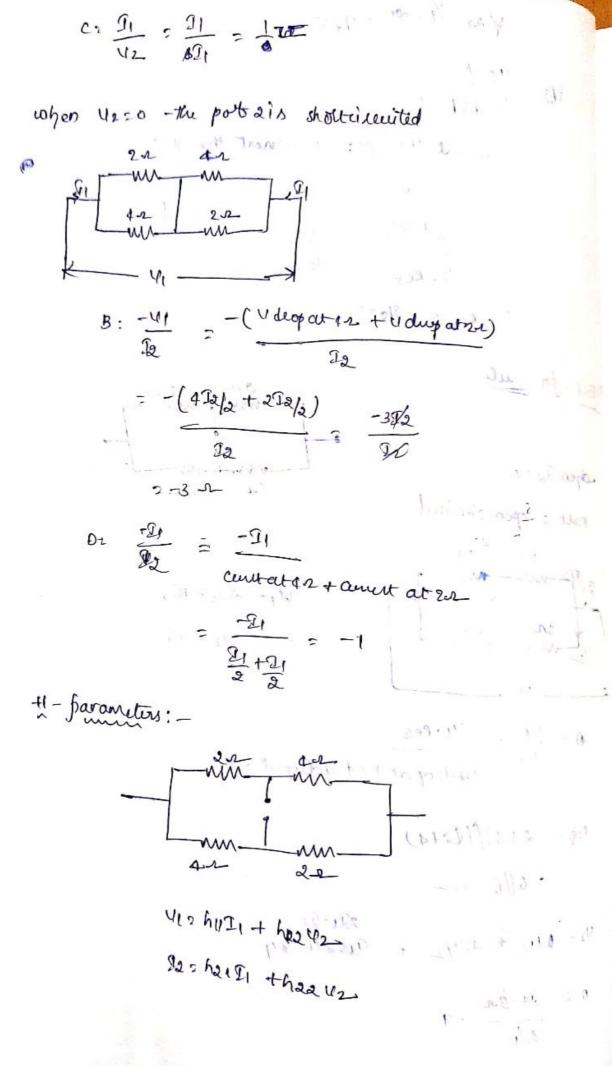
$$= \frac{1}{4} \frac{1}{5} \frac{1}{5}$$

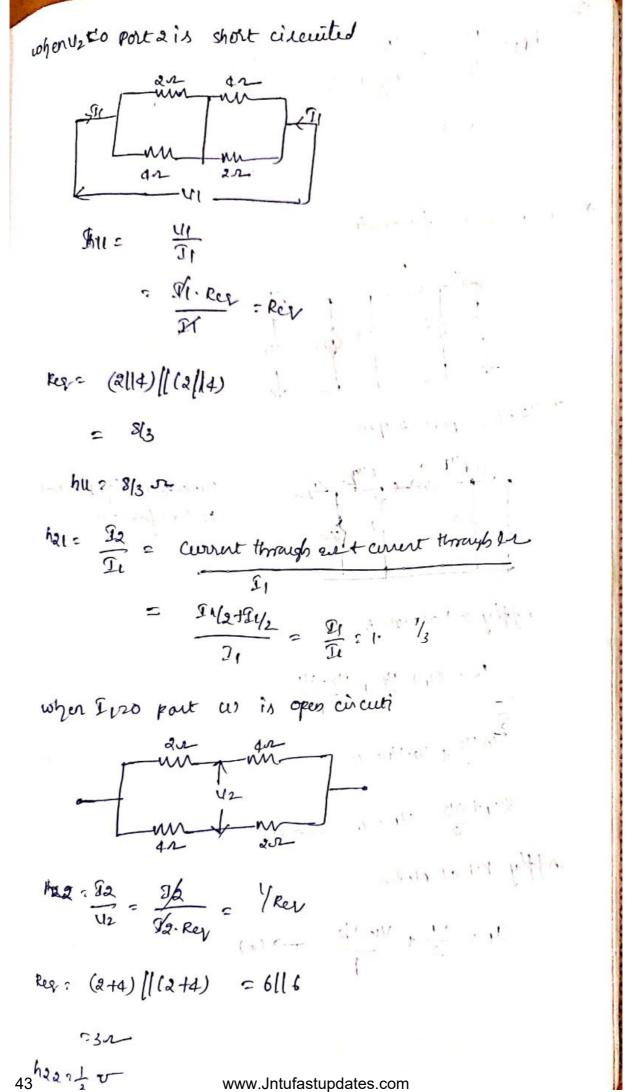
$$Y az \cdot \sqrt{81} = 5 = 51/9 u$$

$$W_{2} = \frac{31}{52} \int \frac{1}{52} \int \frac{1}{52} = 0$$

$$= \frac{1}{52} \int \frac{1}{52} \int \frac{1}{52} = 0$$

$$= \frac{1}{52} \int \frac{1}{52} + \frac{1}{52} \int \frac{1}{52} = \frac{1}{52} \int \frac{1}$$





$$h_{BA}: \frac{g_{12}}{g_{11}} = \frac{g_{12}}{g_{2/2} + g_{1/2}} = \frac{g_{12}}{g_{2/2}}$$

$$find = 2 + \frac{y}{y} - \frac{g_{12}}{g_{1/2} + g_{1/2}} = \frac{g_{12}}{g_{2/2}}$$

$$find = 2 + \frac{y}{y} - \frac{g_{12}}{g_{1/2} + g_{2/2}} = \frac{g_{12}}{g_{2/2}}$$

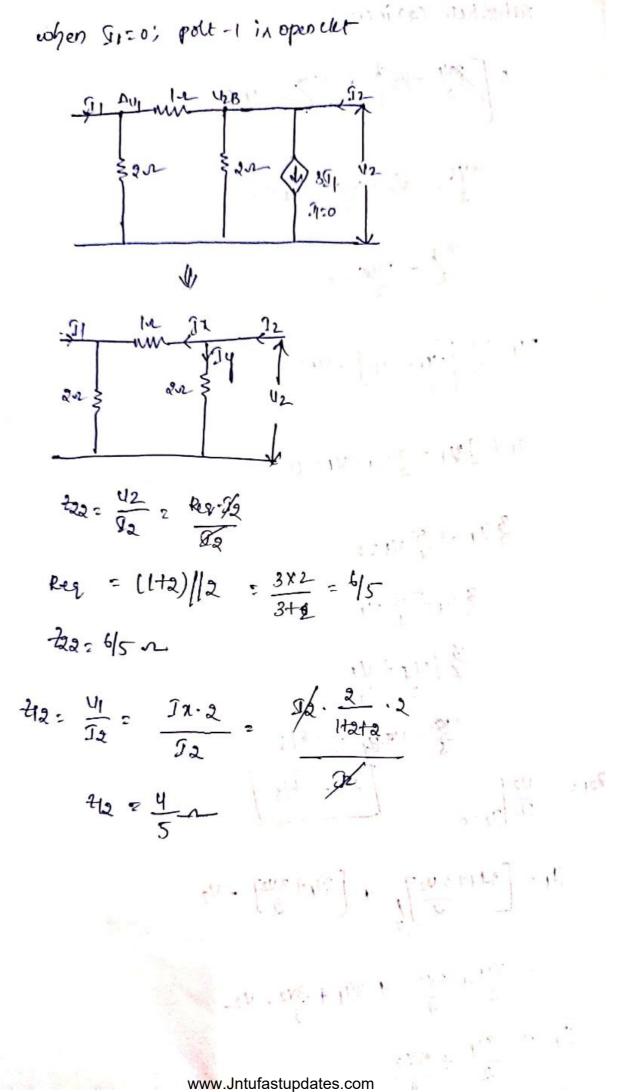
$$h_{BA}: \frac{g_{1}}{g_{1/2}} + \frac{g_{1/2}}{g_{2/2}} = \frac{g_{1/2}}{g_{2/2}} = \frac{g_{1/2}}{g_{2/2}}$$

$$h_{BA}: \frac{g_{1/2}}{g_{1/2}} + \frac{g_{1/2}}{g_{2/2}} = \frac{g_{1/2}}{g_{2/2}} =$$

substitute (2) incu  

$$s \left[ \frac{2}{2} - \frac{1}{2} + \frac{3}{2} + \frac{3}{2} - \frac{1}{2} - \frac{1}{2} + \frac{3}{2} - \frac{1}{2} - \frac{1}{2} + \frac{3}{2} - \frac{1}{2} - \frac{1}{2} + \frac{3}{2} + \frac{3}{2}$$

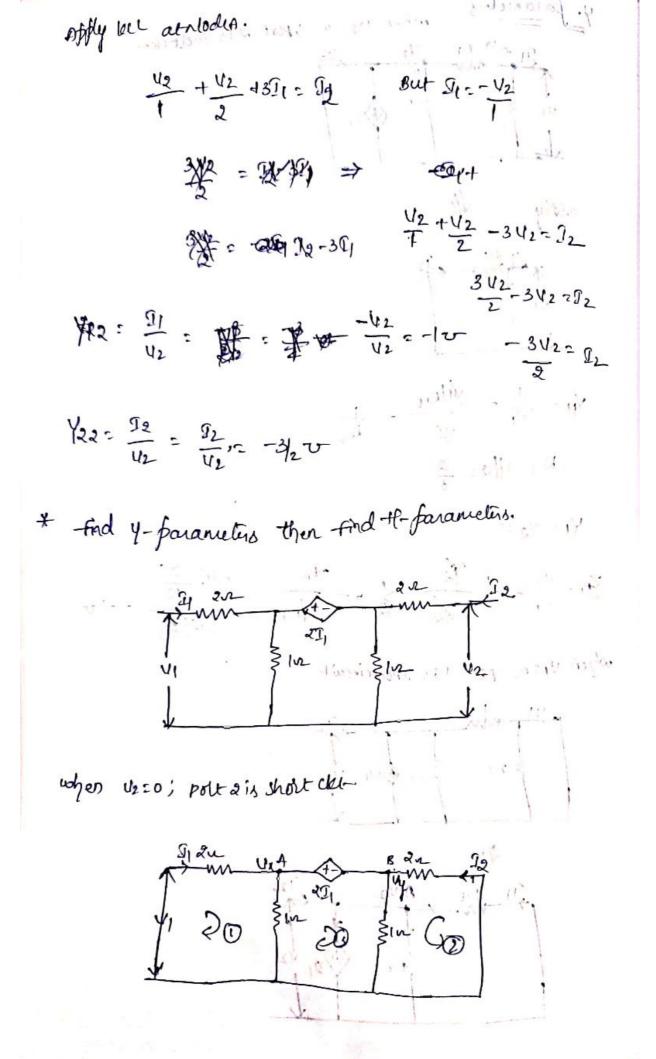
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46

Y- parameters when uzeo ; port-2 is sholtclet J = 22 = 50 D = 51 nopply YII = II = Yilker = 1 yr = ker Regaillaz 2 41,320 1: 12 = 12 = 1 = 1 = 1 = 1 = -1V. H = -1V. H = -1V. when 4120; port-1 is shortcircuit \$ 2n \$521 42 31 www.Jntufastupdates.com

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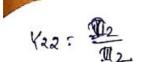




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$$\begin{aligned} & \left\{ 2_{12} := \frac{T_{2}}{V_{1}} \quad \text{using (4)} \quad f(5) := \frac{1}{2} \text{using (4)} \\ & : \frac{1}{2} \text{s}_{1} \right\} \quad \frac{1}{2} \text{s}_{2} := \frac{1}{2} \text{s}_{1} \\ & 181_{2} := \text{u}_{1} \\ & \frac{1}{2} \text{s}_{2} := \frac{1}{18} \text{s}_{1} \\ & \frac{1}{2} \text{s}_{1} := \frac{1}{18} \text{s}_{1} \\ & \frac{1}{2} \text{s}_{1} := \frac{1}{18} \text{s}_{1} \\ & \frac{1}{20} := \frac{1}{20} := \frac{1}{18} \text{s}_{1} \\ & \frac{1}{20} := \frac{1}{20} := \frac{1}{18} \text{s}_{1} \\ & \frac{1}{20} := \frac{1}{20} := \frac{1}{20} := \frac{1}{20} \\ & \frac{1}{20} := \frac{1}{20} := \frac{1}{20} \\$$

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\_51

from egin (2) f (3) 312-3 (-12]= 12 3 J2 + 3 J2 = V2 1812 U2 Y22 2 J2 = 5 -5 KIZ= from esn(2) & (3) = 11 3(-511)-31:002 -1821242 1 42 = II = -1 - J  $h_{11} = \frac{1}{y_{11}} = \frac{18}{5} n \quad h_{21} = \frac{y_{21}}{y_{11}} = \frac{y_{1k}}{51k} = \frac{1}{5}$  $\frac{h_{12}}{y_{11}} = \frac{-(-y_{1y})}{5/y_{1}} + \frac{h_{22}}{5/y_{1}} = \frac{Y_{11}}{y_{11}} + \frac{Y_{12}}{5/y_{1}} + \frac{Y_{11}}{y_{11}} = \frac{Y_{12}}{y_{11}} + \frac{Y_{12}}{y_{11}} = \frac{Y_{12}}{y_{11}} = \frac{Y_{12}}{y_{11}} + \frac{Y_{12}}{y_{11}} = \frac{Y_{12}}{y_{11}}$ = 15 c 4x/54 = 4/5 v

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