

Performance of DC Machines

DC Motors:-

Principle of operation:-



x - into the plane

• - out of the plane

Right hand thumb Rule.

As conductors are placed in ^{the} slots which are on the periphery, the individual force experienced by the conductors acts as a twisting or turning force on the Armature which is called torque.

Torque is the product of force and the radius at which these force acts. so overall Armature experiences a torque and starts rotating.

The magnitude of the force experienced by the conductor in a motor is given by $f = BIl$ [Flux cutting law]

B = Flux density

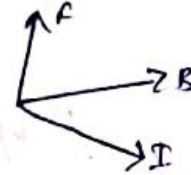
I = current passing through the conductor

l = length of the conductor

The direction of the rotation of the motor can be determined by Fleming's left hand Rule.

thru

Fleming's left hand rule :-



thumb \rightarrow gives direction of force experienced by conductor.

forefinger \rightarrow gives direction of Magnetic field.

Middle finger \rightarrow gives direction of current

* Significance of Back Emf :-

\rightarrow when a current carrying coil is placed in a magnetic field it experiences some force called Torque. This torque is to rotate the armature. The rotated armature cuts the magnetic flux and it induces some emf.

\Rightarrow According to Lenz's law the generated emf opposes the supply voltage. Here the generated emf called back emf.

$$E_b = \frac{\Phi Z N}{60} [P/A]$$

$$N \downarrow$$

$$E_g \propto N \Rightarrow E_g \propto 1$$

$$E_g < E_b$$

$$E_b \downarrow < N \downarrow \Rightarrow (V - E_b) \uparrow \cdot I_a \uparrow \quad T \uparrow \quad N \uparrow$$

* Voltage Equation of a D.C. Motor:-

In a D.C. Motor, supply voltage (V) has to overcome back emf E_b which is opposing the V and also various drops as armature resistance drop $I_a R_a$, brush drop etc.

$$V = E_b + I_a R_a + \text{brush drop}$$

$$I_a = \frac{V - E_b}{R_a}$$

* Power Equation of a DC Motor:-

$$V I_a = E_b I_a + I_a^2 R_a$$

$$P_e = P_m + I_a^2 R_a$$

where P_e is net electrical power input of the armature.

$I_a^2 R_a$ is the power loss due to the resistance of the armature.

P_m is the electrical equivalent of gross mechanical power developed by the armature.

* Condition for maximum power:-

$$E_b I_a = V I_a - I_a^2 R_a$$

$$\text{To get max power, } \frac{dP_m}{dI_a} = 0$$

$$P_m = P_e - I_a^2 R_a$$

$$I_a = \frac{V}{2R_a}$$

$$I_a R_a = \frac{V}{2}$$

Substitute in voltage equation

$$V = E_b + \frac{V}{2}$$

$$\boxed{E_b = \frac{V}{2}}$$

* Torque equation of a DC Motor:-

- It is seen that the turning or twisting force about an axis is called Torque.

- Consider a wheel of radius R acted upon by a circumferential force f newtons, which is shown in the below figure.



- The wheel is rotating at a speed of N rpm.

- The angular speed of the wheel is $\omega = \frac{2\pi N}{60}$ rad/sec

- So work done in one revolution is

$$W = F \times \text{distance travelled in one revolution}$$

$$= f \times 2\pi R \text{ Joules}$$

- Power developed = $\frac{\text{work done}}{\text{time}}$

$$= \frac{f \times 2\pi R}{\text{time for 1 sec}} = \frac{f \times 2\pi R}{60/N}$$

$$= \frac{2fNR}{60} = (f \times R) \left[\frac{2\pi N}{60} \right]$$

$$P = T \times \omega \quad [P = T \times \omega]$$

where T is Torque in Nm:

ω is angular speed in rad/sec

- let T_a be the gross Torque developed by the armature of the motor.

- It is also called armature torque. The gross mechanical power developed in the armature is $E_b I_a$, and seen from the power equation

- So if the speed of the motor is N rpm then power in armature is

$$\text{Power in Arm} = \text{Arm Torque} \times \omega$$

$$E_b I_a = T_a \times \frac{2\pi N}{60}$$

as we know

$$E_b = \frac{\phi Z N}{60} \left[\frac{P}{A} \right]$$

$$\frac{\phi Z N}{60} \cdot \frac{P}{A} \cdot I_a = T_a \times \frac{2\pi N}{60}$$

$$T_a = \frac{\phi I_a Z P}{2\pi A}$$

$$T_a = 0.159 \phi I_a \frac{P Z}{A} \text{ N-m}$$

Different types of D.C. Motors:

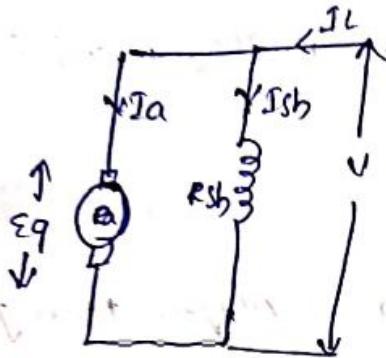
There are 3 types of D.C. Motors.

1. Shunt (D.C) Motor:

3. D.C. Compound motor.

2. D.C. Series Motor

Shunt (D.C) Motor:-



$$I_L = I_{sh} + I_a$$

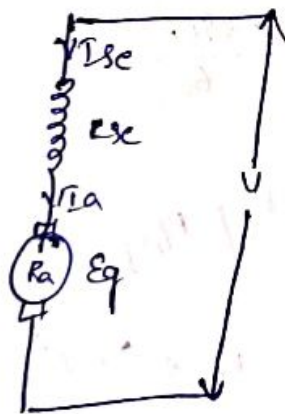
$$V = E_g + I_a R_a$$

$$I_{sh} = \frac{V}{R_{sh}}$$

$$\Phi \propto I_{sh}$$

flux produced by the field winding is proportional to current passing through it.

D.C. Series Motor:-



$$I_L = I_{se} = I_a$$

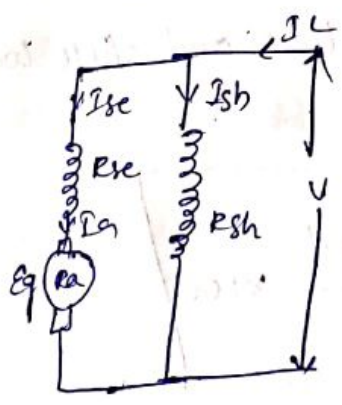
$$V = E_g + I_a R_a + I_{se} R_{se}$$

In series motor entire armature current is passing through the series field winding. So flux produced is proportional to armature current

$$\Phi \propto I_{se} \propto I_a$$

D.C. Compound Motor:-

long shunt

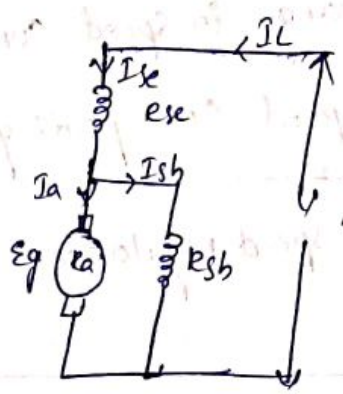


$$I_L = I_{sh} + I_{se}$$

$$I_{sh} = V / R_{sh}$$

$$V = E_g + I_a R_a + I_{se} R_{se}$$

short shunt



$$I_L = I_{se} + I_{sh}$$

$$I_{se} = I_a + I_{sh}$$

$$I_{sh} = \frac{V - I_{se} R_{se}}{R_{sh}}$$

$$V = E_g + I_a R_a + I_{se} R_{se}$$

* Torque and Speed relations:-

$$T = 0.159 \frac{PZ \phi I_a}{A}$$

$$T \propto \phi I_a$$

In shunt field, $T \propto I_a$

In series

$$T \propto \phi I_a$$

$$\phi \propto I_{se}$$

$$T \propto I_{se} I_a$$

$$T \propto I_a^2$$

In series

for series

$$N \propto \frac{V - I_a R_a - I_{se} R_{se}}{\phi}$$

$$E_b = \frac{\phi Z N}{60} \left[\frac{P}{A} \right]$$

$$E_b \propto \phi N$$

$$N \propto \frac{E_b}{\phi}$$

$$E_b = V - I_a R_a$$

$$N \propto \frac{V - I_a R_a}{\phi}$$

* Speed regulation:-

The Speed Regulation for a D.C. Motor is defined as the Ratio of change in speed corresponding to no load and full load condition to speed corresponding to full load.

$$\% \text{ Speed regulation} = \frac{N_{\text{no load}} - N_{\text{full load}}}{N_{\text{full load}}} \times 100$$

* Torque expression in terms of Eb.

$$E_b = \frac{\phi Z N}{60} [P/A]$$

$$\frac{\phi Z P}{A} = \frac{E_b \times 60}{N}$$

$$T = 0.159 \left[\frac{P Z}{A} \right] \phi I_a$$

$$T = \left[\frac{P Z \phi}{A} \right] 0.159 I_a$$

$$T = \frac{E_b \times 60}{N} \times 0.159 I_a$$

$$T = 9.55 \frac{E_b I_a}{N}$$

$$T \propto \frac{1}{N}$$

* shaft torque:-

The torque which is available at the motor shaft for doing useful work is known as shaft torque.

~~Horsepower~~ \rightarrow horsepower = 735.5

* characteristics of a D.C. Motor:-

The characteristics of a DC motor is divided into 3 types:

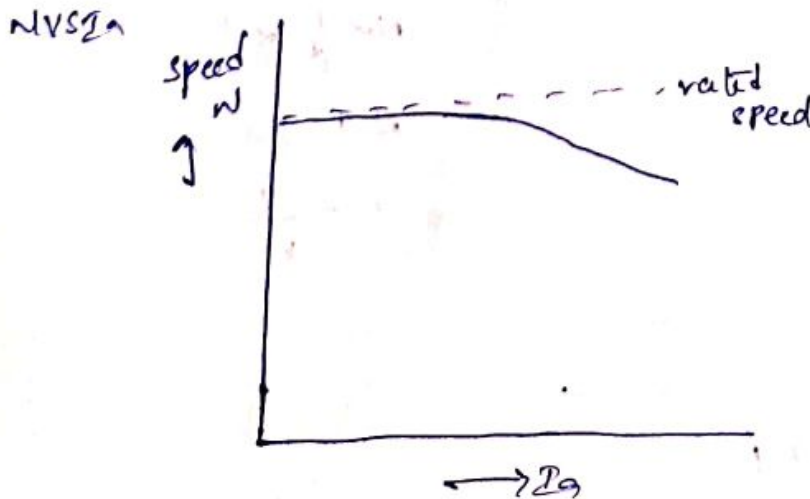
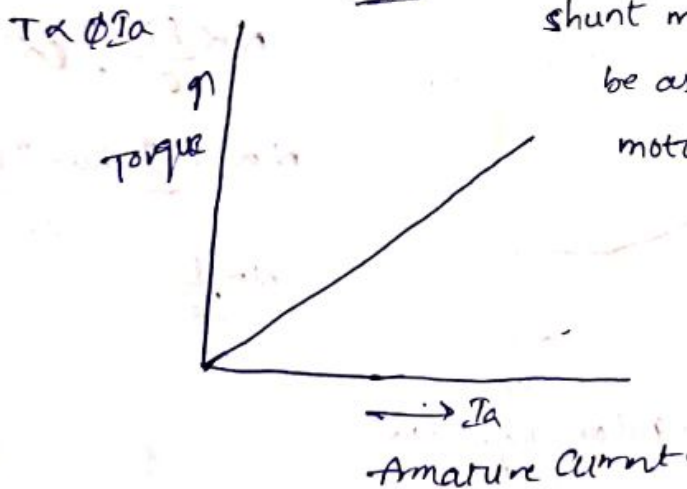
1. Torque vs Armature Current
2. Speed vs Armature Current
3. Speed vs Torque.

DC shunt Motor:-

$$T = 0.159 \frac{PZ^2}{A} \phi I_a$$

ϕ is constant when we apply constant voltage.

shunt motor can be assumed to be as a constant speed motor



$$E_b = \frac{\phi Z N}{60} [P/A]$$

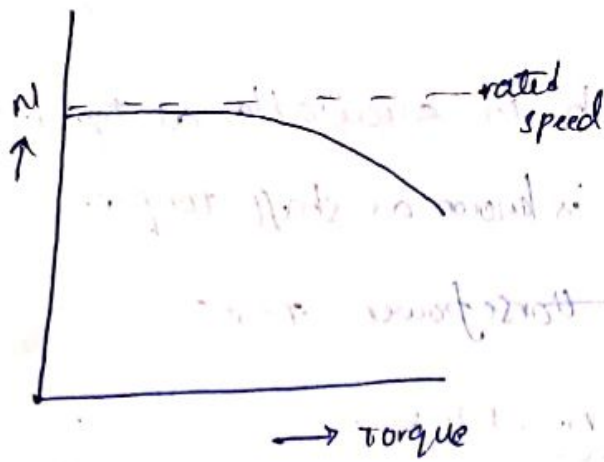
$$E_b = V - I_a R_a$$

$$N \approx \frac{V - I_a R_a}{\phi}$$

Considered as

$$N \approx E_b \text{ (as } \phi \text{ is very less)}$$

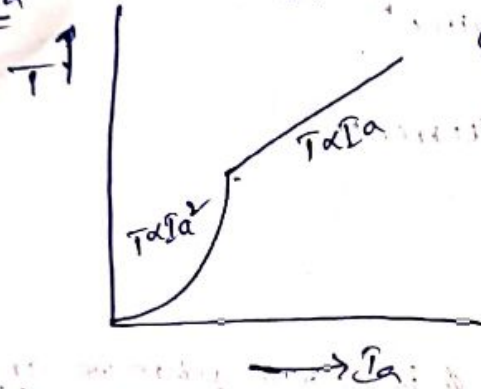
N vs Ia



shunt motor
 $T \propto I_a$
 $T \propto \frac{1}{N}$

* Series Motor

T vs Ia



due to saturation

ϕ will be const.

$$E_b = \frac{\phi Z N}{60} [P/A]$$

$$E_b \propto \phi I_a N$$

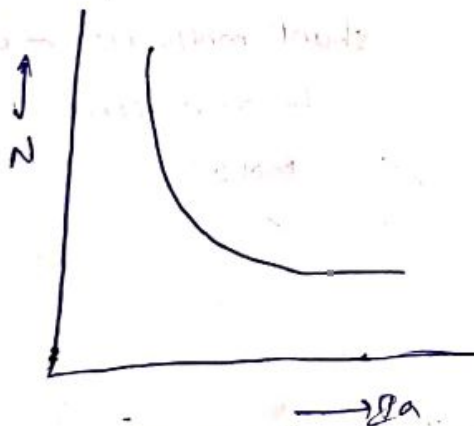
ϕ is varied as core connected

in series with F.W. armature

$$T \propto I_a I_a$$

$$T \propto I_a^2$$

N vs Ia



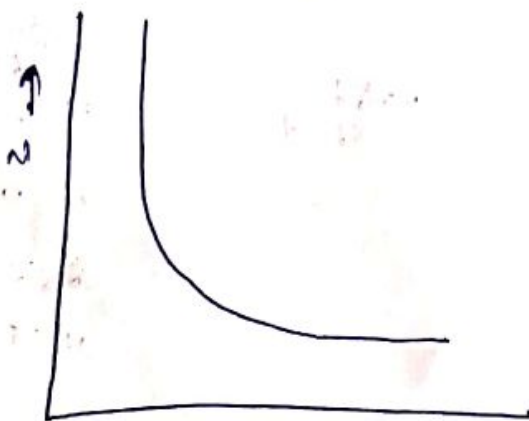
rectangular hyperbola

$$N \propto \frac{E_b}{\phi} \propto \frac{1}{I_a}$$

$$N \propto \frac{V - I_a R_a - I_a R_{se}}{I_a}$$

$$N \propto \frac{1}{I_a}$$

N vs T



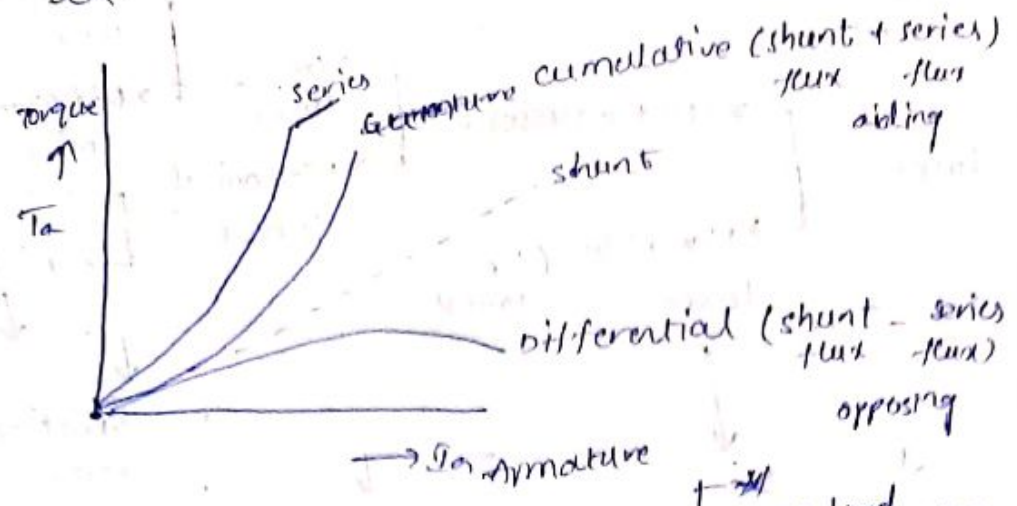
$$N \propto \frac{1}{\phi} \propto \frac{1}{I_a}$$

$$\phi T \propto I_a^2$$

$$N \propto \frac{1}{\sqrt{T}}$$

→ Compound Motor:-

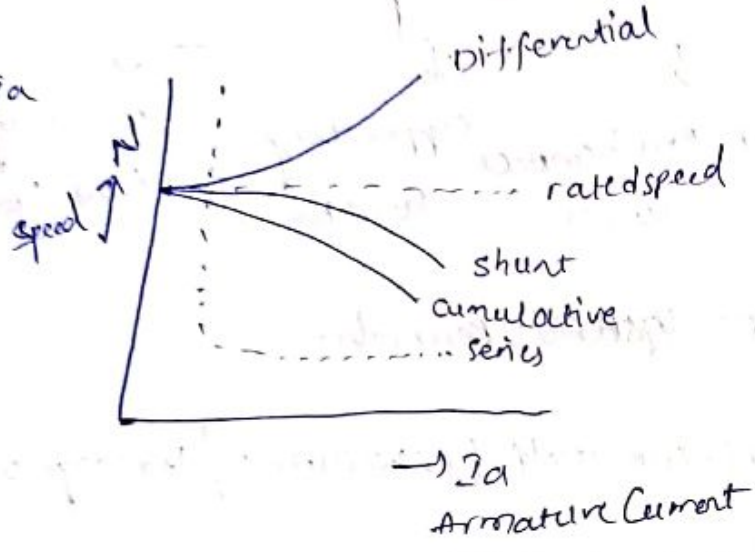
T vs Ia



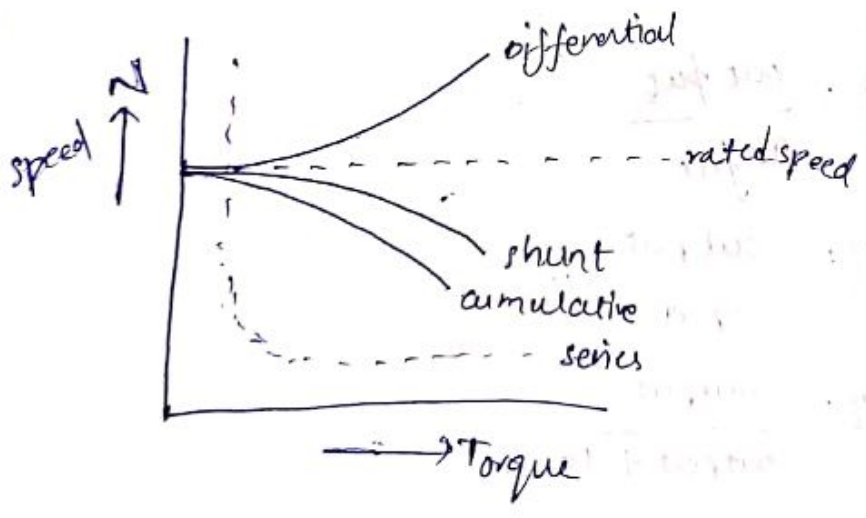
flux aiding
flux opposing

at no load series motor is with high speed

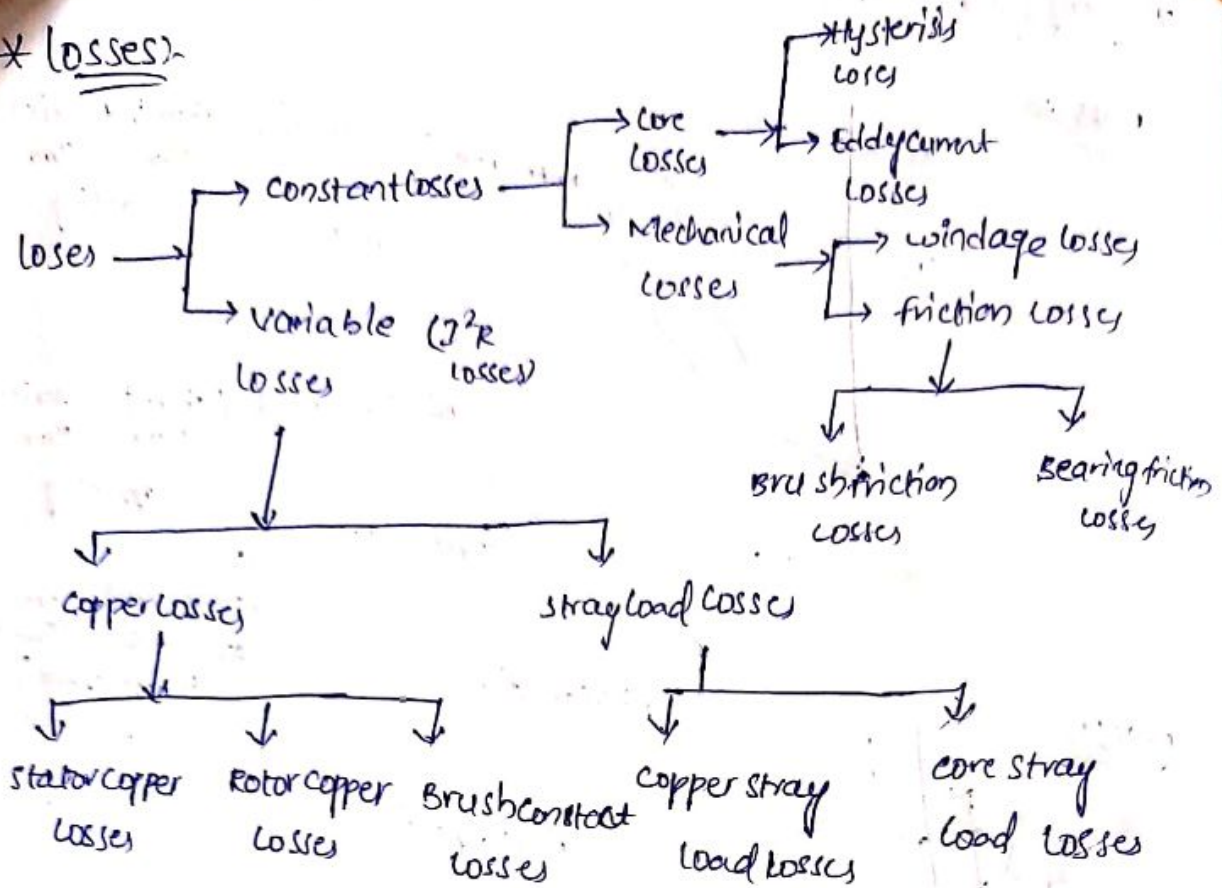
N vs Ia



N vs T



* Losses:-



hysteresis:- Magnetic hysteresis, Reversal.

Eddy currents:- Appear in core itself (extra currents/leakage currents)

Mechanical :- friction due to bolts

* Efficiency (η) :-

$$\eta = \frac{\text{output}}{\text{Input}}$$

$$\% \eta = \frac{\text{output}}{\text{Input}} \times 100$$

$$\eta = \frac{\text{output}}{\text{output} + \text{losses}}$$

$$\eta = \frac{\text{Input} - \text{losses}}{\text{Input}}$$

* A 220V shunt generator supplies a load current of 120A at a rated speed of 800 rpm. The armature and shunt-field resistance are 0.022 and 110 Ω respectively. If the overall efficiency of the machine at this load is 88%. determine armature and shunt-field copper loss.

2- stray losses.

Solⁿ $I_L = 120A$

$N = 800 \text{ rpm}$

Arm. loss = $I_a^2 R_a$

$I_a = I_L + I_{sh}$

$I_{sh} = \frac{V}{R_{sh}} = \frac{220}{110} = 2 \text{ Amp}$

$I_a = 120 + 2 = 122 \text{ Amp}$

Armature current loss = $(122)^2 \cdot 0.022$
 $= 297.7 \text{ W}$

shunt field copper loss = $V \cdot I_{sh}$
 $= 220 \times 2$
 $= 440 \text{ W}$

total copper loss = Armature + shunt-field
 $= 297.7 + 440$
 $= 737.7 \text{ W}$

output of generator = $V \cdot I_L = 220 \times 120$
 $= 26400 \text{ W}$

$$\text{Mechanical Input} = \frac{\text{output}}{\text{Efficiency}}$$

$$= \frac{26400}{0.88} = 301000 \text{ W}$$

$$\text{Total losses} = \text{output input} - \text{output}$$

$$= 301000 - 26400$$

$$= 3600 \text{ W}$$

$$\text{stray load losses} = \text{total losses} - \text{copper loss}$$

$$= 3600 - 737.7$$

$$= 2862.32 \text{ W}$$

* The following data pertain to a short shunt compound generator

$$\text{Armature resistance} = 0.04 \Omega$$

$$\text{Series field resistance} = 0.025 \Omega$$

$$\text{shunt field resistance} = 45 \Omega$$

$$\text{Contact drop per brush} = 1 \text{ V}$$

$$\text{Magnetic losses} = 2.5 \text{ kW}$$

$$\text{Mechanical losses} = 1 \text{ kW}$$

find the efficiency of the generator when it delivers 400 A at 440 V

sol:- Armature $R_a = 0.04 \Omega$

$$R_{se} = 0.025$$

$$R_{sh} = 45 \Omega$$

M_a

$$\text{voltage across shunt field winding} = V + I R_{se}$$

$$= 440 + 400 \times 0.025$$

$$= 450 \text{ V}$$

$$I_{sh} = \frac{V}{R_{sh}} = \frac{450}{45}$$

$$= 10 \text{ Amp}$$

$$I_a = I_L + I_{sh}$$

$$= 450 + 10$$

$$= 460 \text{ amp}$$

$$\text{Amature copper loss} = I_a^2 R_a = (460)^2 \times 0.04$$

$$= 8,724 \text{ W}$$

$$\text{series field copper loss} = I^2 R_{se} = (400)^2 \times 0.025$$

$$= 4000 \text{ W}$$

$$\text{shunt field copper loss} = V \cdot I_{sh} = 450 \times 10 = 4500 \text{ W}$$

$$\text{brush contact loss} = 2 \times I_a$$

$$= 2 \times 460$$

$$= 920 \text{ W}$$

$$\text{total losses} = \text{Amature} + \text{series field} + \text{shunt field} + \text{brush} \\ + \text{Mech} + \text{Mag}$$

$$= 8724 + 4000 + 920 + 4500 + 2500 + 1000$$

$$= 19544 \text{ W}$$

$$\text{out put} = V \times I$$

$$= 440 \times 400$$

$$= 176000 \text{ W}$$

$$\% \text{ Efficiency } \eta = \frac{\text{output}}{\text{output} + \text{loss}}$$

$$= \frac{176000}{176000 + 19544}$$

$$= \frac{176000}{195544}$$

$$= 0.9 \times 100$$

$$= 90\%$$

* A 440V shunt motor has armature resistance of 0.8Ω and field resistance of 200Ω . Determine the back emf when giving an output of 7.46 kW at efficiency 85%.

sd:-
=

$$V = 440\text{V}$$

$$R_a = 0.8\Omega$$

$$\text{Output} = 7.46 \text{ kW}$$

$$\eta = 85\%$$

$$R_{sh} = 200\Omega$$

$$E_b = ?$$

$$\text{Power input} = \frac{\text{output}}{\eta}$$

$$= \frac{7.46 \times 10^3}{0.85} = \frac{8776.47}{0.85} = 10325.26 \text{ W}$$

we know that $E_b = V - I_a R_a$

$$I_a = I_L + I_{sh}$$

$$I_L = \frac{V}{R_f} = \frac{440}{\frac{1}{0.027 \times 10^3}} = \frac{440}{8776.47} = 0.05 \text{ A}$$

$$I_{sh} = \frac{V}{R_{sh}} = \frac{440}{200} = 2.2 \text{ A}$$

$$I_a = 5089.67 \text{ A} - 0.05 \text{ A} = 5089.62 \text{ A}$$

$$19.95 - 2.2 = 17.75 \text{ A}$$

$$E_b = 440 - 17.75 \times 0.8$$

$$= 440 - 14.2$$

$$= 425.8 \text{ V}$$

* find the useful flux per pole on load of 200V, 6 pole shunt motor having a wave connected armature winding with 110 turns. the armature resistance is 0.2Ω. The armature current is 13.3A at the no-load speed of 908 rpm.

Solⁿ

$$\phi = ?$$

$$N = 908 \text{ rpm}$$

$$Z = 110 \times 2$$

$$= 220$$

$$A = 2$$

$$P = 6$$

$$V = 250$$

$$R_a = 0.2$$

$$I_a = 13.3$$

$$E_b = \frac{\phi Z N}{60} \left[\frac{P}{A} \right]$$

$$E_b = V - I_a R_a$$

$$= 250 - (13.3 \times 0.2)$$

$$= 247.34 \text{ V}$$

$$247.34 = \frac{\phi \times 220 \times 908}{60} \left[\frac{6}{2} \right]$$

$$= \phi \times 9988$$

$$\phi = 24.7 \text{ mWb}$$

* A 250V, shunt motor on no-load runs at 1000rpm and takes 5amp. the total armature and shunt field resistances are 0.2Ω and 250Ω respectively. calculate the speed when loaded and taking current of 50amp. if armature reaction weakens the field by 3%.

Sol:

$$V = 250 \text{ V} \quad R_{sh} = 250$$

$$N = 1000$$

$$I_L = 5$$

$$R_a = 0.22$$

$$I_a = 50$$

Armature reaction: 9%

at no load condition

$$I_a = I_L - I_{sh}$$

$$I_{sh} = \frac{V}{R_{sh}} = \frac{250}{250} = 1$$

$$I_a = 5 - 1 = 4 \text{ A}$$

$$E_{b1} = 250 - 4 \times 0.2$$

$$= 249.2 \text{ V}$$

$$\frac{E_{b2}}{E_{b1}} = \frac{\Phi_2 N_2}{\Phi_1 N_1}$$

$$n_2 = \frac{E_{b2}}{E_{b1}} \times \frac{\Phi_1 N_1}{\Phi_2}$$

$$= \frac{249.2 \times 1 \times 1000}{249.2 \times 0.97}$$

$$= 994 \text{ rpm}$$

at loaded condition

$$I_L = 50$$

$$I_a = I_L - I_{sh} = 50 - 1 = 49 \text{ A}$$

$$E_{b2} = V - I_a R_a$$

$$= 250 - 49 \times 0.2$$

$$= 240.2 \text{ V}$$

* A 6-pole DC Motor has a wave connected Armature with 87-slots, each slot containing 6 conductors. The flux per pole is 30mWb and the armature has a resistance of 0.1Ω . Calculate the speed when the motor is connected to a 250V supply, and taking an armature current of 80amp. Calculate also the torque in N-m, developed by the armature.

Sol:

$$P = 6, A = 2$$

$$Z = 87 \times 6 = 522$$

$$\phi = 30\text{mWb} = 0.03$$

$$R_a = 0.1\Omega$$

$$N = ?$$

$$V = 250\text{V}$$

$$I_a = 80$$

$$E_b = V - I_a R_a$$

$$= 250 - 80 \times 0.1$$

$$= 250 - 8$$

$$= 242\text{V}$$

$$E_b = \frac{\phi Z N}{60} \left[\frac{P}{A} \right]$$

$$N = \frac{E_b \times 60 \times A}{\phi \times Z \times P}$$

$$= \frac{242 \times 60 \times 2}{0.03 \times 522 \times 6}$$

$$= 310\text{rpm}$$

$$\text{Torque } T_a = 0.159 \times \phi \times I_a \times \frac{PZ}{A} \quad (\text{or}) \quad 9.55 \times \frac{E_b I_a}{N}$$

$$= 0.159 \times 0.03 \times 80 \times \frac{6 \times 522}{2}$$

$$= 597.58\text{ N-m}$$

* A four pole 250 V series motor has a wave connected Armature with 1254 conductors. The flux per pole is 22 mWb when the motor is taking 50 A. Iron and friction losses amount to 1.0 kW and armature resistance is 0.2 Ω and series field resistance is 0.2 Ω, calculate BHP (Break Horse power), speed, shaft torque / useful torque.

sol:- $P = 4, A = 2$ $I_L = 50$ $V = 250$
 $Z = 1254$, $\phi = 22 \times 10^{-3}$ $R_a = 0.2 \Omega$
 friction losses = 1000 W , $R_{se} = 0.2 \Omega$

$$I_L = I_{se} = I_a$$

$$E_b = \frac{\phi Z N}{60} \left[\frac{P}{A} \right]$$

$$E_b = V - I_a R_a - I_{se} R_{se}$$

$$= 250 - 50 \times 0.2 - 50 \times 0.2$$

$$= 240 \text{ V} - 10 = 230 \text{ V}$$

$$230 = \frac{22 \times 10^{-3} \times 1254 \times N}{60} \left[\frac{4}{2} \right]$$

$$230 = 0.919 \times N$$

$$N = 250 \text{ rpm}$$

1) total resistance = $R_a + R_{se}$

$$= 0.2 + 0.2$$

$$= 0.4$$

Mechanical power developed in the armature

$$= V I_a$$

$$\text{Mech power developed} = VI_a - I_a^2 (R_a + R_{se})$$

$$= 250 \times 50 - (50)^2 (0.4)$$

$$P_m = 11500 \text{ W}$$

useful power: $P_m - \text{Iron and friction losses}$

$$= 11500 - 1000$$

$$= 10,500 \text{ W}$$

$$\text{useful power } P_m = \frac{2\pi n I T_{\text{shaft}}}{60}$$

$$10500 = \frac{2\pi \times 250 \times T}{60}$$

$$10500 = 26.18 \times T$$

$$T = 399.8 \text{ N-m}$$

$$T_{sh} = 401 \text{ N-m}$$

$$\text{BHP} = \frac{10500}{746} = 14.075 \text{ HP}$$

A 250V, 4-pole shunt motor has two circuit armature winding with 500 conductors. The armature circuit resistance is 0.25Ω field resistance is 125Ω and flux per pole 0.02wb . Neglect armature reaction. Find the speed and torque developed if the motor draws 14A from the mains.

solⁿ $V = 250$, $A = 2$, (wave connected = two circuit armature)

$$P = 4, Z = 500, R_a = 0.25, R_{sh} = 125, \phi = 0.02$$

$$I_L = 14$$

$$E_b = \frac{\phi Z N}{60} [P/A]$$

$$I_a = I_L - I_{sh} = 14 - 2 = 12\text{A}$$

$$E_b = V - I_a R_a = 250 - 12 \times 0.25 = 247\text{V}$$

$$N = \frac{E_b \times 60 \times A}{\phi \times Z \times P} = \frac{247 \times 60 \times 2}{0.02 \times 500 \times 4}$$

$$= 741\text{rpm}$$

$$E_b I_a = \frac{2\pi N T}{60}$$

$$247 \times 12 = \frac{2\pi \times 741 \times T}{60}$$

$$T = 38.19\text{N-m}$$

* Determine the torque developed when a current of 30A passes through armature of a motor with the following particulars lap winding, 310 conductors, 4-poles, pole shoes 16.2 cm long subtending an angle 60° at the centre, Bore radius 16.2 cm, flux density in the airgap $b = 0.7$ Tesla.

Sol:-

$$T = 0.159 \Phi I_a \left[\frac{ZP}{A} \right]$$

$$I_a = 30 \quad A = 4$$

$$Z = 310$$

$$P = 4$$

$$D = 2R = 2 \times 16.2$$

$$= 2 \times 16.2$$

$$= 32.4 \text{ cm}$$

$$B = 0.7 \text{ T}$$

$$\text{pole arc} = \left[\frac{60}{360} \right] \pi D$$

$$= \frac{\pi D}{6} = \frac{\pi \times 32.4}{6} = 16.9 \text{ cm}$$

Flux per pole = flux density \times pole arc \times core length

$$= 0.7 \times 16.9 \times 16.2 \text{ cm}$$

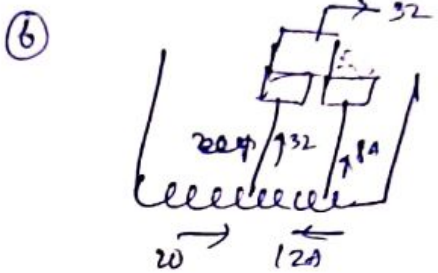
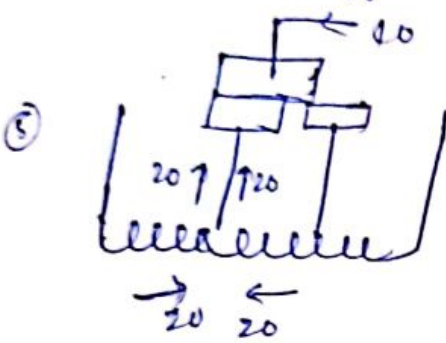
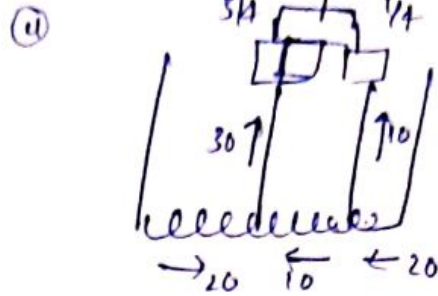
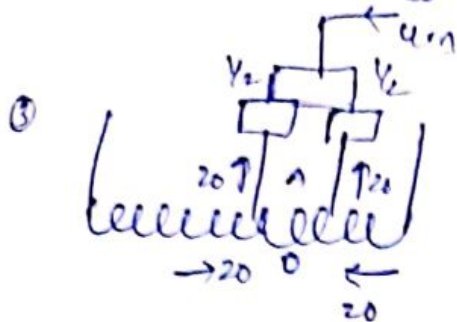
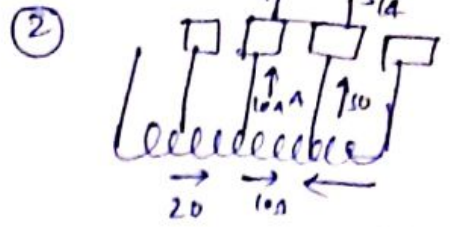
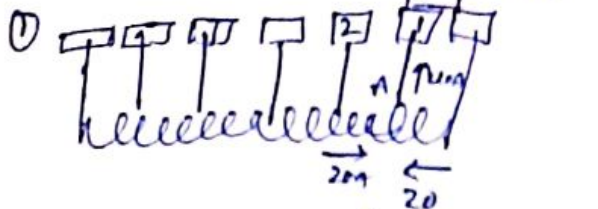
$$= 0.7 \times 0.169 \times 0.162 \text{ m}$$

$$= 0.0193 \text{ wb}$$

$$T = \frac{0.159 \times 0.0193 \times 30 \times 310 \times 4}{4}$$

$$= 28.5$$

Commutation:-



$$\text{commutation period} = \frac{wb - wm}{v}$$

$$\text{Rebance voltage} = L \times \frac{2I}{T_c}$$

w_b = brush width

w_m = insulation width (mica)

