

* check the following conditions.

1. static, dynamic
2. Linear, Non-linear
3. causal, non-causal
4. time invariant, variant

1. $y(n) = x(n) - 5x(n-1)$

5. $y(n) = a^{x(n)}$

2. $y(n) = x(2n)$

6. $y(n) = |x(n)|$

3. $y(n) = x(n/3)$

7. $y(n) = \log(1 + |x(n)|)$

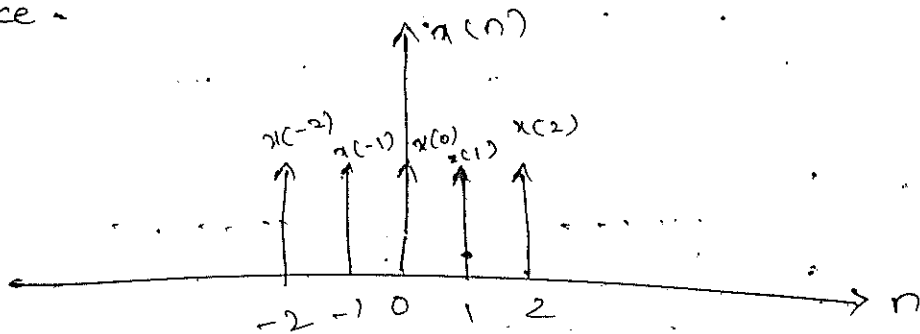
4. $y(n) = x(n) \cdot \cos\left(\frac{\pi n}{6}\right)$

14) 7/10/06

Arbitrary Representation of a Sequence:-

Any sequence can be represented as sum of shifted version of unit sample sequences is called arbitrary representation of a sequence.

Ex:-



$$x(n) = \dots + x(-2)\delta(n+2) + x(-1)\delta(n+1) + x(0)\delta(n) + x(1)\delta(n-1) + x(2)\delta(n-2) + \dots$$

$$x(n) = \sum_{k=-\infty}^{\infty} x(k)\delta(n-k)$$

Linear Time-Invariant System (or) Discrete time linear time-invariant system :-

LTI (or) DTLTI system:

A discrete time system it satisfies

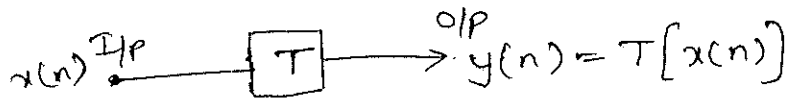
the following properties

- (i) Linearity Property
- (ii) Time invariant Property.

Properties:

① LTI System response (or) Convolution Sum :-

Any discrete time system can be represented mathematically as



where $x(n)$ is given as excitation and $y(n)$ is the response of the system.

- If the unit sample sequence is given to the input of the system i.e; $x(n) = \delta(n)$, then the response of the system is called impulse response, i.e; $y(n) = T[x(n)]$.

$$y(n) \Big|_{x(n) = \delta(n)} = h(n) = T[\delta(n)]$$

- Generally, response of the system is

$$y(n) = T[x(n)]$$

∴ w.k.T arbitrary rep. of $x(n)$ summation is

$$x(n) = \sum_{k=-\infty}^{\infty} x(k) \delta(n-k)$$

$$y(n) = T \left[\sum_{k=-\infty}^{\infty} x(k) \delta(n-k) \right] \quad \text{--- (1)}$$

In LTI system, it satisfies linearity property.

By using linearity property, eq. (1) reduces to

$$y(n) = \sum_{k=-\infty}^{\infty} x(k) T[\delta(n-k)]$$

An LTI system also satisfies time-invariant property

Impulse response due to shifted impulse sequence is

$$h[n, k] = T[\delta(n-k)]$$

$$\therefore y(n) = \sum_{k=-\infty}^{\infty} x(k) \cdot h(n, k)$$

It satisfies time in-variant property.

$$\text{Then } h(n, k) = h(n-k)$$

★

$$\therefore y(n) = \sum_{k=-\infty}^{\infty} x(k) \cdot h(n-k) \text{ which is called as}$$

response of LTI system. $\leftarrow y(n) = x(n) * h(n)$ ★

② causality of LTI system :-

causality :-

A discrete time system is said to be causal if its output at any instant of time, n depends on present input, past input and output samples but does not depend on future input samples.

The necessary and sufficient condition for causality of LTI system is

$$h(n) = 0 \text{ for } n < 0$$

Pf :- w.k.T the $y(n) = \sum_{k=-\infty}^{\infty} x(k)h(n-k) = x(n) * h(n)$

It satisfies commutative property.

$$y(n) = \sum_{k=-\infty}^{\infty} h(k)x(n-k) = h(n) * x(n).$$

\Rightarrow

$$y(n) = \dots + h(-2)x(n+2) + h(-1)x(n+1) + h(0)x(n) + h(1)x(n-1) + \dots$$

A system

The above equation satisfies causality only when

$$h(-1) = h(-2) = h(-3) = \dots = 0$$

i.e; $h(n) = 0$ for $n < 0$.

\therefore The above equation satisfies causality.

Response of causality of LTI system is

$$y(n) = h(0)x(n) + h(1)x(n-1) + \dots$$

$$y(n) = \sum_{k=0}^{\infty} h(k)x(n-k)$$

③ Condition for stability of LTI system:-

STABILITY:-

Any arbitrary relaxed system is said to be BIBO stable iff every bounded input yields bounded output.

The necessary and sufficient condition for stability of LTI system is

$$\sum_{k=-\infty}^{\infty} |h(k)| < \infty$$

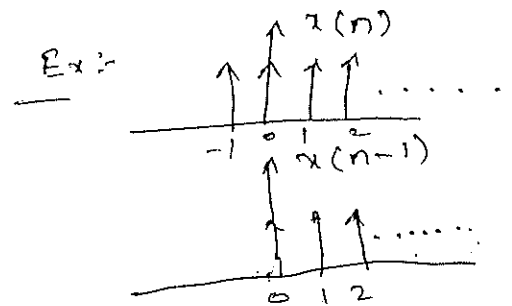
Pf:- we know that the response of LTI system is

$$y(n) = \sum_{k=-\infty}^{\infty} h(k) \cdot x(n-k)$$

for stable condition, the input is bounded such that the ~~magnitude~~.

$$|x(n)| = M_x$$

$$\therefore |x(n-k)| = M_x$$



~~y(n) =~~

Apply magnitude (or) absolute value on the both sides of absolute equation

$$|y(n)| = \left| \sum_{k=-\infty}^{\infty} h(k) x(n-k) \right|$$

w.k.T magnitude of sum of terms is always less than sum of magnitudes.

$$\text{i.e., } |y(n)| = \left| \sum_{k=-\infty}^{\infty} h(k) x(n-k) \right| \leq \sum_{k=-\infty}^{\infty} |h(k)| |x(n-k)|$$

[∵ |a+b| ≤ |a|+|b|]

$$|y(n)| \leq \sum_{k=-\infty}^{\infty} |h(k)| M_x$$

$$|y(n)| \leq M_x \sum_{k=-\infty}^{\infty} |h(k)|$$

The above eq. is stable and has finite value only

if $\sum_{k=-\infty}^{\infty} |h(k)| < \infty$

* Test whether the following systems are causal or not and stable or not.

1. $y(n) = \cos(x(n))$

2. $y(n) = a x(n)$

3. $y(n) = a^{x(n)}$

4. $y(n) = x(n) e^n$

5. $y(n) = \sum_{k=-\infty}^{\infty} x(k)$

→ (i) $y(n) = \cos(x(n))$

$y(n) \Big|_{x(n)=\delta(n)} = h(n) = \cos(\delta(n))$

$n=0$	$h(0) = \cos(\delta(0)) = \cos(1) = 0.54$	$n=-1$	$h(-1) = \cos(\delta(-1)) = \cos(0) = 1$
$n=1$	$h(1) = \cos(\delta(1)) = \cos(0) = 1$		$= \cos(0) = 1$
$n=2$	$h(2) = \cos(\delta(2)) = \cos(0) = 1$		\vdots

(i) Causality:

From this,

$h(-1) = h(-2) = \dots = 1$

$\therefore h(n) \neq 0$ for $n < 0$

So the system is non-causal.

(ii) Stability.

Condition for stability of LTI system is

$$\sum_{n=-\infty}^{\infty} |h(n)| < \infty$$

$$\sum_{n=-\infty}^{\infty} |h(n)| = \dots + |h(-1)| + |h(0)| + |h(1)| + \dots$$

$$= \dots + 1 + 1 + 0.5a + 1 + 1 + \dots$$

$$= \infty$$

$\therefore \sum_{n=-\infty}^{\infty} |h(n)| < \infty$ \therefore system is non-stable.

② $y(n) = a x(n)$

$$y(n) \Big|_{x(n)=\delta(n)} = h(n) = a \delta(n)$$

$$\begin{array}{l|l} n=0 & h(0) = a \delta(0) = a \\ n=1 & h(1) = a \delta(1) = 0 \\ n=2 & h(2) = a \delta(2) = 0 \\ & \vdots \end{array} \quad \begin{array}{l|l} n=-1 & h(-1) = a \delta(-1) = 0 \\ & \vdots \\ & \vdots \end{array}$$

(i) From this,

$$h(-1) = h(-2) = \dots = 0$$

$\therefore h(n) = 0$ for $n < 0$

\therefore system is causal.

$$(ii) \sum_{n=-\infty}^{\infty} h(n) = \dots + h(-1) + h(0) + h(1) + \dots$$

$$= 0 + 0 + \dots + a + 0 + 0 + \dots$$

$$= \underline{a} < \infty$$

\therefore system is stable.

③ $y(n) = a^{x(n)}$

$$y(n) \Big|_{x(n)=\delta(n)} = h(n) = a^{\delta(n)}$$

$$\begin{array}{l|l} n=0 & h(0) = a^{\delta(0)} = a \\ n=1 & h(1) = a^0 = 1 \\ & \vdots \end{array} \quad \begin{array}{l|l} n=-1 & h(-1) = a^0 = 1 \\ & \vdots \\ & \vdots \end{array}$$

$$\therefore h(-1) = h(-2) = \dots = 1$$

$\therefore h(n) \neq 0$ for $n < 0$. \therefore It is non-causal.

$$\sum_{n=-\infty}^{\infty} h(n) = \dots + 1 + 1 + \dots + a + 1 + 1 + \dots$$

$$= \infty$$

\therefore It is unstable system.

$$\textcircled{4} \quad y(n) = x(n) e^n$$

$$\rightarrow y(n) \Big|_{x(n)=\delta(n)} = h(n) = \delta(n) e^n$$

$$x(n) = \delta(n)$$

$$\begin{array}{l} n=0 \\ n=1 \\ \vdots \end{array} \left| \begin{array}{l} h(0) = \delta(0) e^0 = 1 \\ h(1) = \delta(1) e^1 = 0 \\ \vdots \end{array} \right| \quad \begin{array}{l} n=-1 \Rightarrow h(-1) = \delta(-1) e^{-1} = 0 \\ \vdots \end{array}$$

$\therefore h(n) = 0$ for $n < 0$ \therefore causal system.

$$\sum_{n=-\infty}^{\infty} h(n) = 1 + 0 + 0 + \dots$$

$$= 1 < \infty$$

\therefore It is stable system.

$$\textcircled{5} \quad y(n) = \sum_{k=-\infty}^{n+1} x(k)$$

$$\rightarrow y(n) \Big|_{x(n)=\delta(n)} = h(n) = \sum_{k=-\infty}^{n+1} \delta(k)$$

$$x(n) = \delta(n)$$

$$= \dots + \delta(-1) + \delta(0) + \delta(1) + \dots$$

$$\dots + \delta(n) + \delta(n+1)$$

$$\begin{aligned}
 n=0 \quad | \quad h(0) &= \dots + \delta(-2) + \delta(-1) + \delta(0) + \delta(1) + \dots + \delta(\infty) + \delta(-\infty) \\
 &= \sum_{k=-\infty}^{0+1} \delta(k) \\
 &= \sum_{k=-\infty}^1 \delta(k) = 0 + 0 + 1 + 0 + \dots \\
 &= \underline{\underline{1}}
 \end{aligned}$$

$$n=1 \Rightarrow h(1) = \sum_{k=-\infty}^2 \delta(k) = \underline{\underline{1}}$$

$$\vdots$$

$$n=-1 \Rightarrow h(-1) = \sum_{k=-\infty}^0 \delta(k) = \underline{\underline{1}}$$

$$n=-2 \Rightarrow h(-2) = \sum_{k=-\infty}^{-1} \delta(k) = 0$$

$$\vdots$$

$\therefore h(n) = 1 \neq 0$ for $n < 0$.

\therefore The given system is non-causal system.

$$\sum_{n=-\infty}^{\infty} h(n) = \dots + 1 + 1 + 1 + \dots = \infty$$

\therefore It is unstable system.

① $h(n) = 2^n u(-n)$ ③ $h(n) = \delta(n) + \sin(n\pi)$

② $h(n) = \sin\left(\frac{n\pi}{2}\right)$ ④ $h(n) = e^{2n} u(n-1)$

\rightarrow ① $h(n) = 2^n u(-n)$

$n=0 \Rightarrow h(0) = 2^0 u(0) = \underline{\underline{1}}$ $n=1 \Rightarrow h(1) = 2 u(1) = 0$ \vdots	$n=-1 \Rightarrow h(-1) = 2^{-1} u(-1) = 1/2$ $n=-2 \Rightarrow h(-2) = 2^{-2} u(-2) = 1/4$ \vdots
--	--

$$\therefore h(n) = \frac{1}{2} + \frac{1}{4} + \dots \neq 0 \text{ for } n < 0$$

\therefore It is non-causal system.

$$\begin{aligned} \sum_{n=-\infty}^{\infty} |h(n)| &= \sum_{n=-\infty}^{\infty} |2^n u(-n)| \\ &= \sum_{n=-\infty}^{\infty} 2^n |u(-n)| \\ &= \sum_{n=-\infty}^0 2^n |u(-n)| + \sum_{n=1}^{\infty} 2^n |u(-n)| \end{aligned}$$

$$u(-n) = \begin{cases} 1 & \text{for } -n \geq 0 \\ & n \leq 0 \\ 0 & \text{for } n > 0. \end{cases}$$

$$= \sum_{n=-\infty}^0 2^n (1) + 0$$

$$= \sum_{n=-\infty}^0 2^n$$

Put $n = -k$

$$n \rightarrow -\infty \Rightarrow k \rightarrow \infty$$

$$n \rightarrow 0 \Rightarrow k \rightarrow 0$$

$$\begin{aligned} \therefore \sum_{n=-\infty}^{\infty} h(n) &= \sum_{k=\infty}^0 \frac{1}{2^k} \\ &= \sum_{k=0}^{\infty} \frac{1}{2^k} \end{aligned}$$

$$= \sum_{k=0}^{\infty} \left(\frac{1}{2}\right)^k$$

$$= \frac{1}{1 - \frac{1}{2}} = \underline{\underline{2}}$$

\therefore It is finite, hence it is stable system.

$$\textcircled{2} \quad h(n) = \sin\left(\frac{n\pi}{2}\right)$$

* Find the convolution b/w the following two sequences by the graphical method.

$$x(n) = \{1, 2, 3, 1\} ; \quad h(n) = \{1, 2, 1, -1\}$$

\uparrow \uparrow \uparrow \uparrow
 0 1 2 3

NOTE :-

① If $x(n)$ starts at $n = n_x$

$h(n)$ starts at $n = n_h$, then

the convolution output $y(n)$ starts at $n = n_x + n_h$

② If $x(n)$ ends at $n = n_{x1}$

$h(n)$ ends at $n = n_{h1}$, then

$y(n)$ ends at $n = n_{x1} + n_{h1}$

③ If the length of the sequence $x(n)$ is N_1 , and the length of $h(n)$ sequence is N_2 ;

then convolution output $y(n)$ is $N_1 + N_2 - 1$.

$$\rightarrow y(n) \text{ starts at } n = 0 + (-1) = -1$$

$$y(n) \text{ ends at } n = n_{x1} + n_{h1} = 3 + 2 = 5$$

$$\begin{aligned} \text{length of the o/p } y(n) &= N_1 + N_2 - 1 \\ &= 4 + 4 - 1 \\ &= 7 \end{aligned}$$

LTI System response is

$$y(n) = \sum_{k=-\infty}^{\infty} x(k) h(n-k) = x(n) * h(n)$$

$y(n)$ starts at $n = -1$

$$\therefore \text{ At } n = -1 ; y(-1) = \sum_{k=-\infty}^{\infty} x(k) h(-1-k)$$

$$n = 0 ; y(0) = \sum_{k=-\infty}^{\infty} x(k) h(-k)$$

$$n = 1 ; y(1) = \sum_{k=-\infty}^{\infty} x(k) h(1-k)$$

At $n=2$; $y(2) = \sum_{k=-\infty}^{\infty} x(k)h(2-k)$

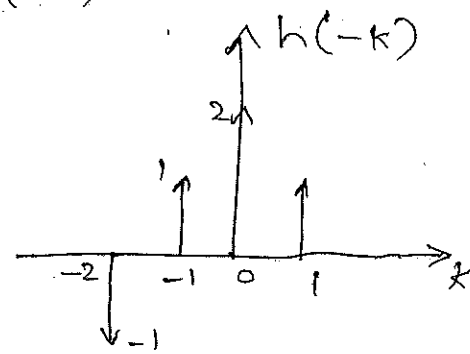
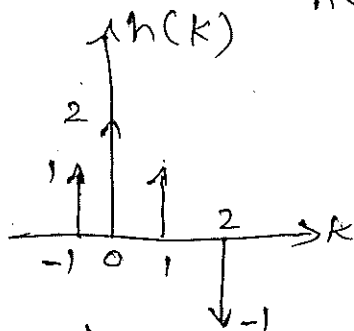
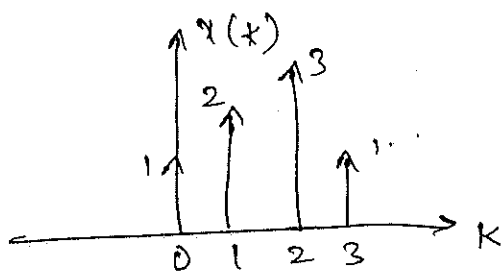
$n=3$; $y(3) = \sum_{k=-\infty}^{\infty} x(k)h(3-k)$

$n=4$; $y(4) = \sum_{k=-\infty}^{\infty} x(k)h(4-k)$

$n=5$; $y(5) = \sum_{k=-\infty}^{\infty} x(k)h(5-k)$

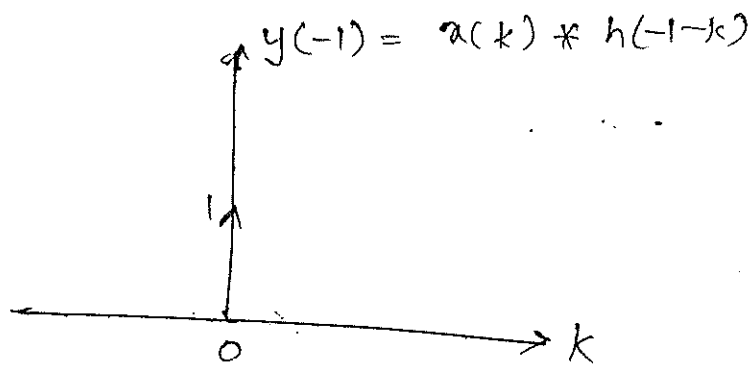
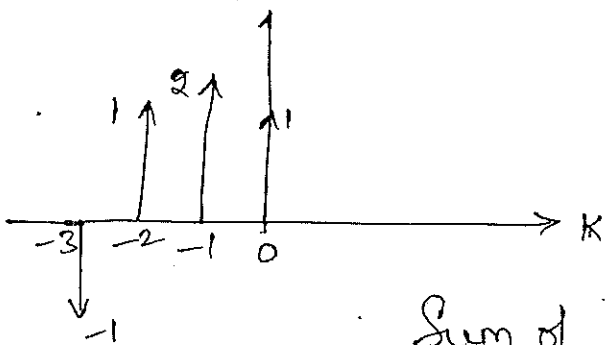
Graphically,

$h(-1-k) = h(-(1+k))$



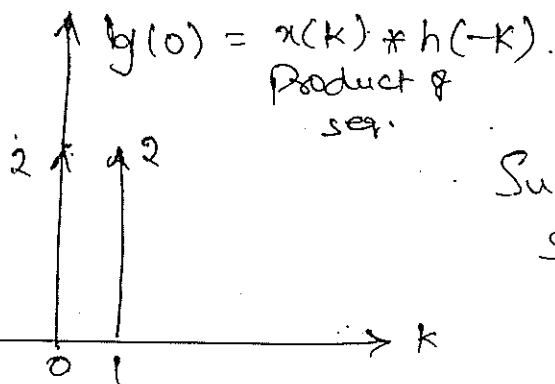
Computation of $y(-1)$ value

$h(-1+k)$



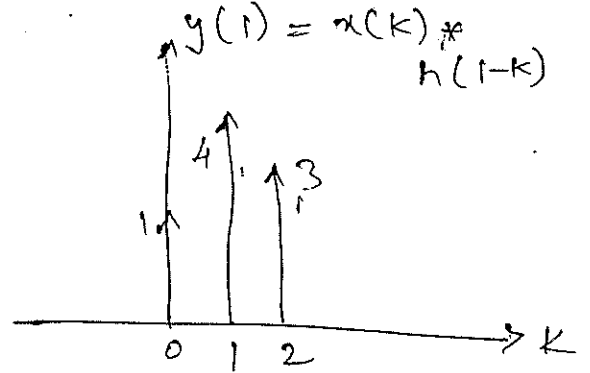
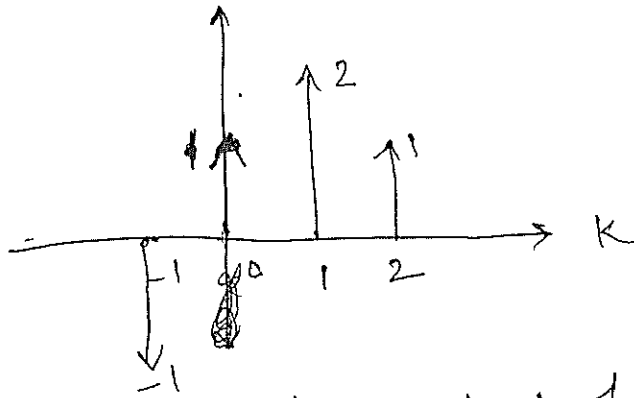
Sum of product of sequence = $y(-1) = 1 = \underline{\underline{1}}$

$y(0)$:-



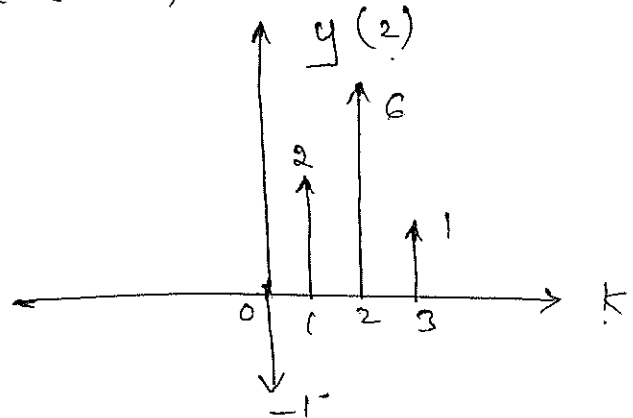
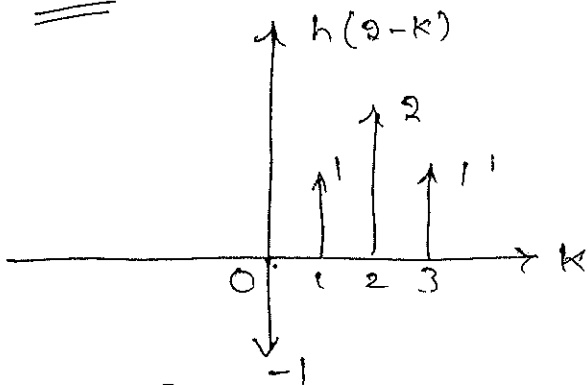
Sum of product of sequences
= $2+2 = \underline{\underline{4}}$

$y(1) := h(1-k) = h(-(k-1))$



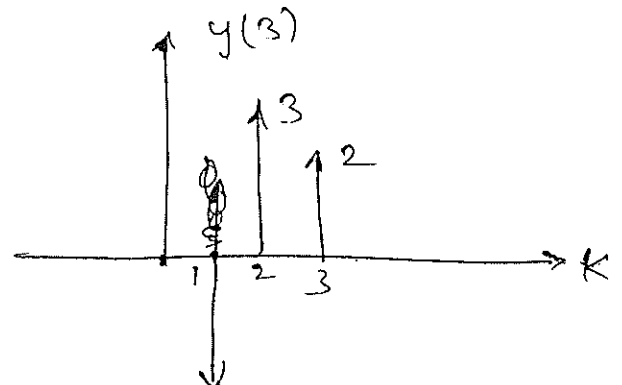
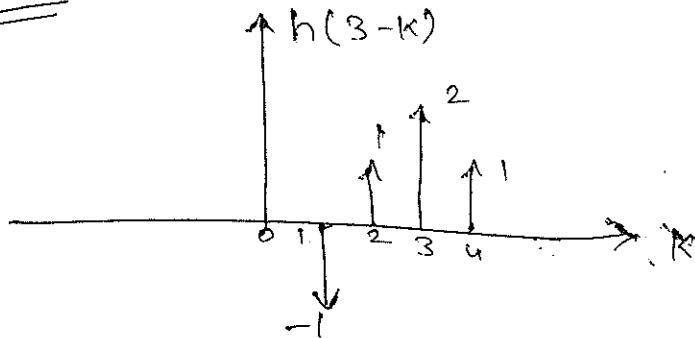
Sum of product of sequences = $1 + 4 + 3 = \underline{\underline{8}}$

$y(2) := h(2-k) = h(-(k-2))$



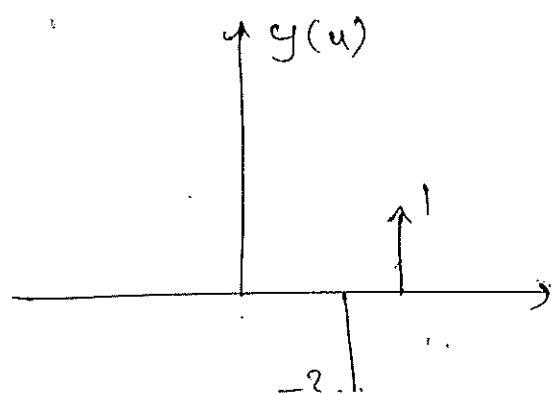
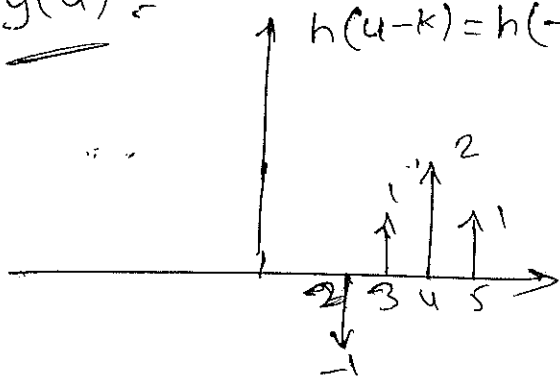
Sum of product of sequences = $-1 + 2 + 6 + 1 = \underline{\underline{8}}$

$y(3) := h(3-k) = h(-(k-3))$



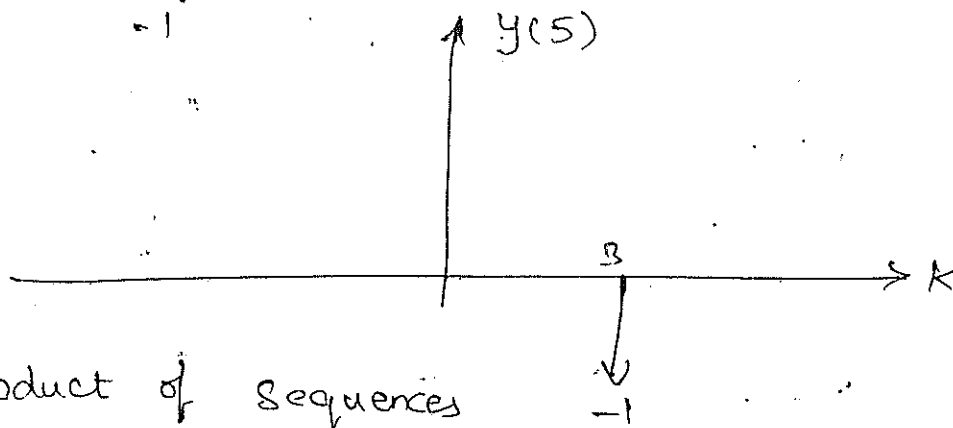
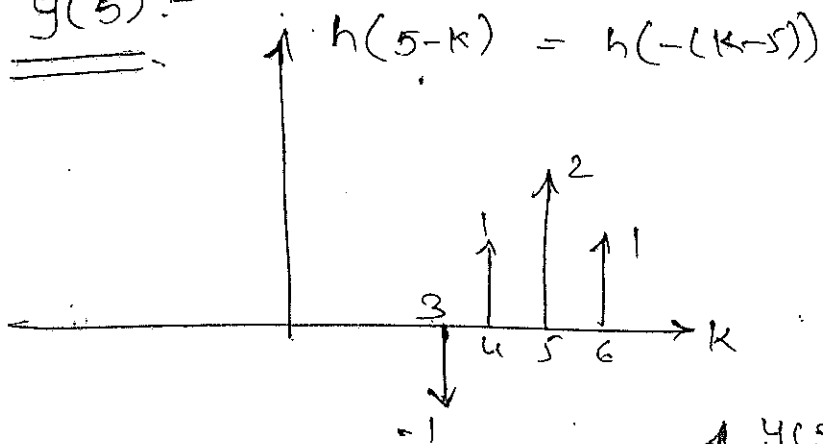
Product of sequences = $-2 + 3 + 2 = \underline{\underline{3}}$

$y(4) := h(4-k) = h(-(k-4))$



Product of sequences = $-3 + 1 = \underline{\underline{-2}}$

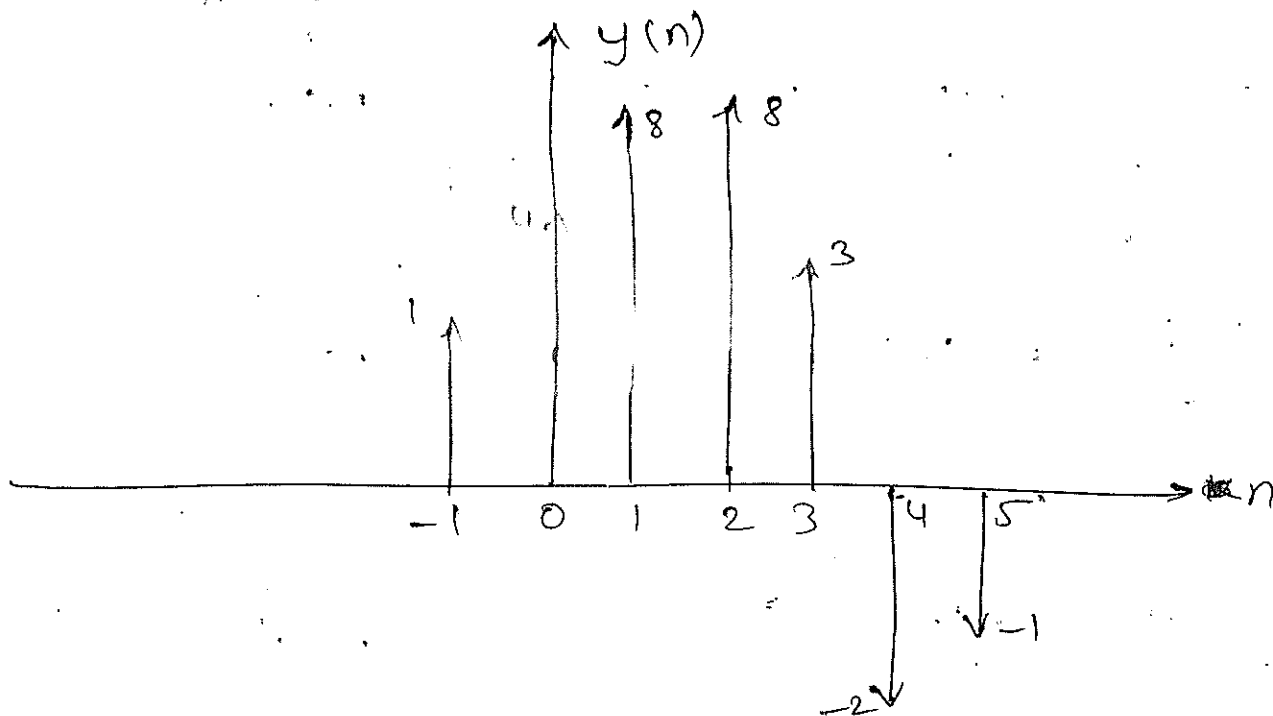
$y(5)$:-



∴ Product of sequences
= $\underline{\underline{-1}}$

∴ $y(n) = \{ 1, 4, 8, 8, 3, -2, -1 \}$

Graphically, $y(n)$ is



Verification method:-

	$x(n) \rightarrow$	1	2	3	1
$h(n) \downarrow$	1	1	2	3	1
	2	2	4	6	2
	1	1	2	3	1
	-1	-1	-2	-3	-1

$y(-1) = 1$

$y(0) = 2+2=4$

$y(1) = 1+4+3 = 8$

$y(2) = -1+2+6+1 = 8$

$y(3) = -2+3+2 = 3$

$y(4) = -3+1 = -2$

$y(5) = -1$

H.W

(1)

$x_1(n) = \{1, 2, -3, -2\}$

↑

$x_2(n) = \{-1, 0, -1, 2\}$

↑

		1	2	-3	2
-1		-1	0	3	2
0		0	0	0	0
-1		-1	-2	3	2
2		2	4	-6	-4

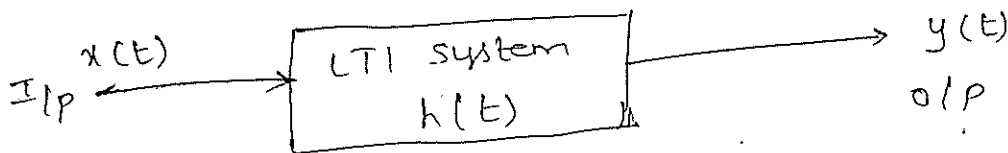
M/3/6c.

UNIT - IV

SIGNAL TRANSMISSION THROUGH SYSTEMS.

Transfer function of LTI System:-

If the continuous time signal $x(t)$ is given to the I/P of an LTI system, $h(t)$ is unit sample response of LTI system, then the response of system is as shown in the figure.



$$y(t) = x(t) * h(t) = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau$$

$$y(t) = h(t) * x(t) = \int_{-\infty}^{\infty} h(\tau) x(t-\tau) d\tau$$

Apply F.T on both sides,

$$F[y(t)] = F[x(t) * h(t)]$$

w.k.T $y(t) \longleftrightarrow Y(\omega)$

$$x(t) \longleftrightarrow X(\omega)$$

$$h(t) \longleftrightarrow H(\omega)$$

and $g_1(t) * g_2(t) \longleftrightarrow F[g_1(t)] \cdot F[g_2(t)]$

$$\longleftrightarrow G_1(\omega) G_2(\omega)$$

$$Y(\omega) = F[x(t)] \cdot F[h(t)]$$

$$= X(\omega) \cdot H(\omega)$$

$$H(\omega) = \frac{Y(\omega)}{X(\omega)}$$

The transfer fn. of the system defined by ~~ratio~~ the ratio of F.T of o/p signal to the F.T of I/P signal.

$$T.F = \boxed{H(\omega) = \frac{Y(\omega)}{X(\omega)}} = \frac{\text{o/p polynomial in } \omega}{\text{I/p Polynomial in } \omega}$$

where $H(\omega) = |H(\omega)| e^{j\angle H(\omega)}$

$|H(\omega)|$ — magnitude spectrum of the system.

$\angle H(\omega)$ — phase " " " "

$X(\omega) = |X(\omega)| e^{j\angle X(\omega)}$ — I/P freq. Spectrum.

$Y(\omega) = |Y(\omega)| e^{j\angle Y(\omega)}$ — o/p " "

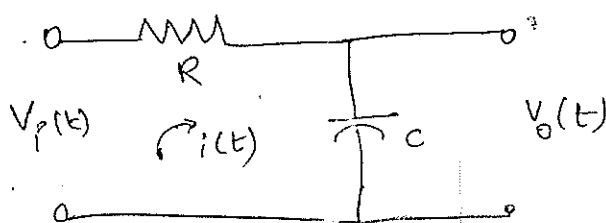
$$\begin{aligned} |Y(\omega)| e^{j\angle Y(\omega)} &= |X(\omega)| e^{j\angle X(\omega)} \cdot |H(\omega)| e^{j\angle H(\omega)} \\ &= |X(\omega)| \cdot |H(\omega)| e^{j[\angle X(\omega) + \angle H(\omega)]} \end{aligned}$$

$$\therefore \boxed{\begin{aligned} |Y(\omega)| &= |X(\omega)| \cdot |H(\omega)| \quad \text{and} \\ \angle Y(\omega) &= \angle X(\omega) + \angle H(\omega) \end{aligned}}$$

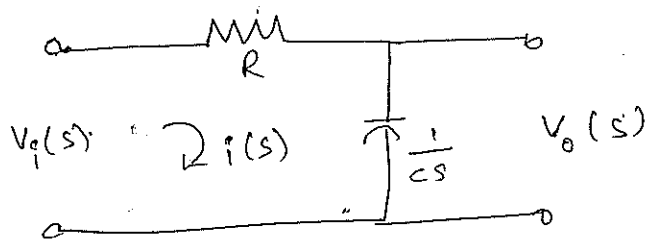
The system transfer fn's changes with input spectral characteristics in amplitude and phase functions.

Filter characteristics of linear systems :- ★

Consider a RC-low pass filter as shown in figure.



Equivalent Laplace transform circuit is



$$V_i(s) = \left(R + \frac{1}{cs}\right) I(s) \quad ; \quad V_o(s) = \frac{1}{cs} I(s)$$

$$H(s) = \frac{V_o(s)}{V_i(s)} = \frac{1/cs}{R + 1/cs} = \frac{1}{1 + sRC}$$

$$\mathcal{L}^{-1}\{H(s)\} = \mathcal{L}^{-1}\left\{\frac{1}{RC\left(\frac{1}{RC} + s\right)}\right\}$$

$$\Rightarrow h(t) = \frac{1}{RC} e^{-t/RC} u(t)$$

ω-k-T $e^{-at} u(t) \leftrightarrow \frac{1}{a + j\omega}$

$e^{at} u(t) \leftrightarrow \frac{1}{a - j\omega}$

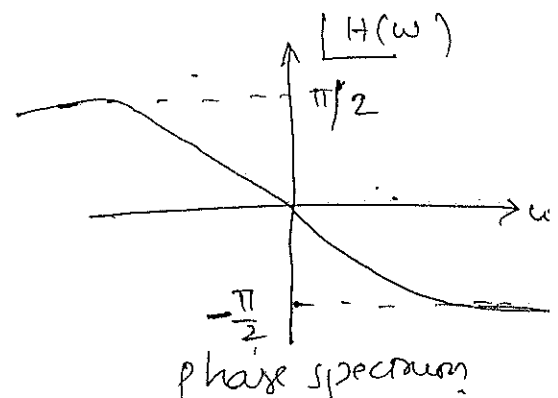
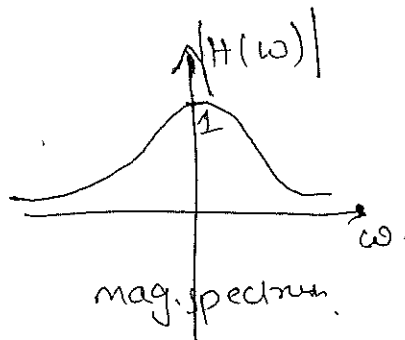
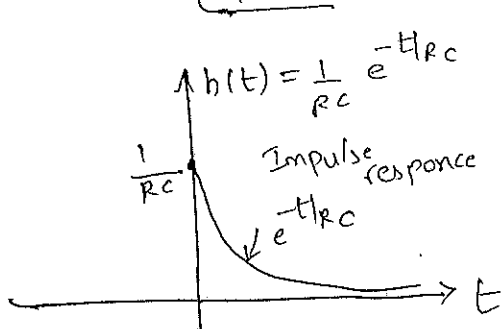
$\frac{1}{RC} e^{-t/RC} u(t) \leftrightarrow \frac{1}{RC} \frac{1}{\frac{1}{RC} + j\omega}$

$h(t) = \frac{1}{RC} e^{-t/RC} u(t) \leftrightarrow \frac{1}{1 + j\omega RC} = H(\omega)$

$$\therefore H(\omega) = \frac{1}{1 + j\omega RC}$$

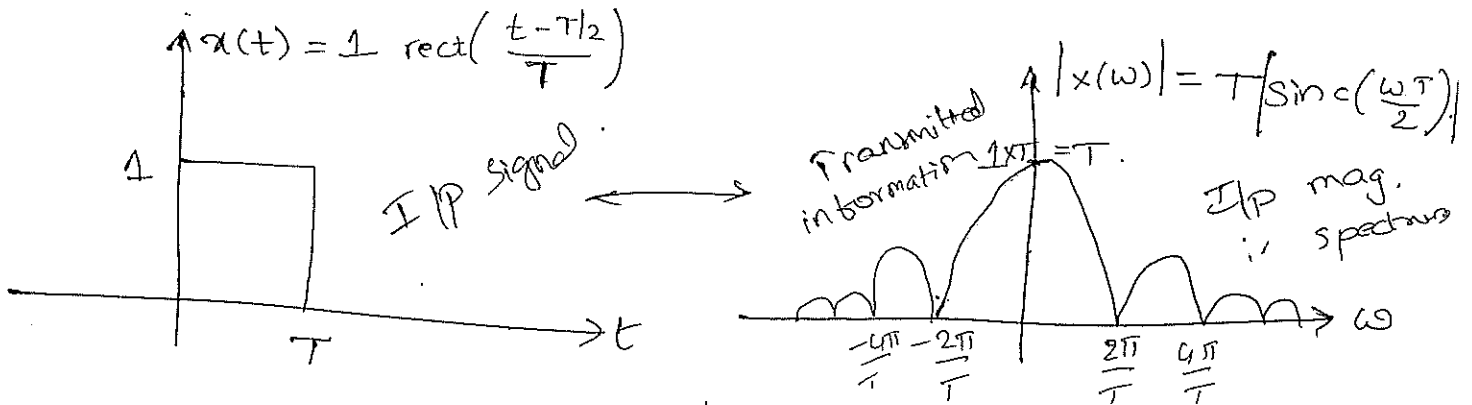
$|H(\omega)| = \frac{1}{\sqrt{1 + \omega^2 RC^2}} \rightarrow$ system magnitude spectrum

$\angle H(\omega) = -\tan^{-1}(\omega RC)$ - Phase spectrum



Let us discuss how

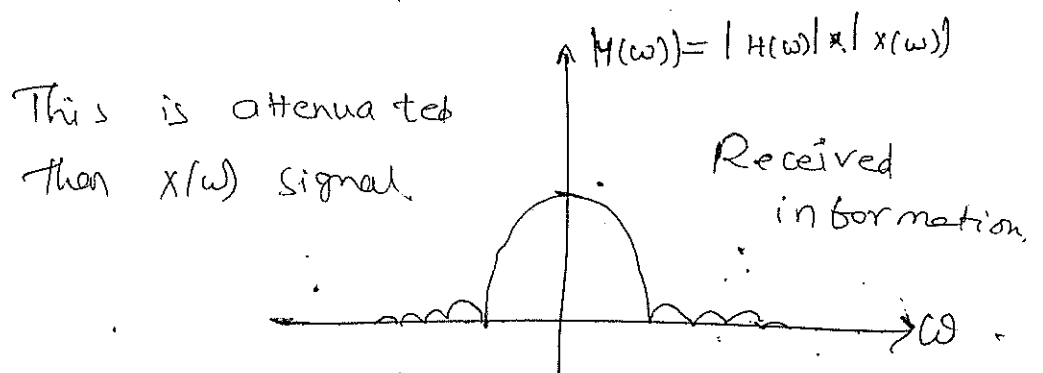
The filter characteristics $|H(\omega)|$ will be changed for the response of the ~~the~~ system due to rectangular I/P signal.



When we pass the ^{rectangular} I/P signal through a low pass filter, low pass filter allows ^(*) only low frequency components of I/P signal and ~~is~~ attenuates high frequency components of I/P signal.

i.e., the I/P signal is filtered by the factor of $|H(\omega)|$ and the output phase is combination of input phase and system phase.

The o/p in time domain and freq. domains are as shown in below



Distortion less transmission through a system:-

The o/p of communication channel is exactly replica of the I/P signal except permissible change of constant amplitude and, constant time delay.

- ~~the~~ the I/P signal ~~(t)~~ $x(t)$ is transmitted through a system is distortion less, if the o/p of the

system satisfies the following conditions:-

$$y(t) = kx(t - t_0)$$

where 'k' is constant independent of frequency.

t_0 - Constant time delay.

$x(t)$ - Transmitted I/P signal; $y(t)$ - Received o/p signal.

This ~~which~~ is condition for distortionless system in t-domain.

In freq. - domain;

$$F[y(t)] = F[kx(t - t_0)]$$

w.k.T

$$y(t) \leftrightarrow Y(\omega)$$

$$x(t) \leftrightarrow X(\omega)$$

$$x(t - t_0) \leftrightarrow e^{-j\omega t_0} X(\omega)$$

$$Y(\omega) = k e^{-j\omega t_0} X(\omega)$$

w.k.T

$$Y(\omega) = H(\omega) \cdot X(\omega)$$

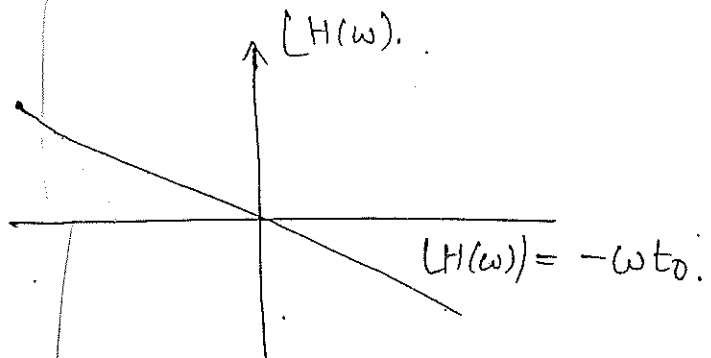
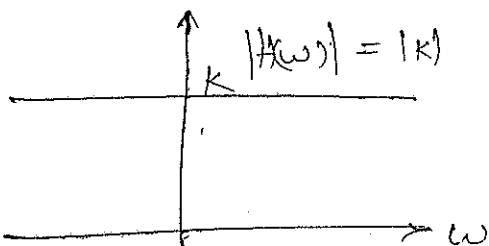
$\therefore H(\omega) = k e^{-j\omega t_0}$ which is condition for distortionless system in f-domain.

From this equation, it is seen that any signal is transmitted through distortionless system, the following conditions ~~are~~ must be satisfied.

(i) $|H(\omega)| = |k| |e^{-j\omega t_0}| = |k|$ - System mag. Spectrum

(ii) $\angle H(\omega) = -\omega t_0$ - Phase Spectrum.

Graphically,



Condition 3 :-

(i) The system is distortionless, System transfer function magnitude f_n must be constant.

(ii) The system is distortionless, the system transfer f_n , phase f_n ^{must} linearly vary with frequency.

= General distortionless transfer function 'H'

$$H(\omega) = K \exp[j(-\omega t_0 + n\pi)] \quad n \text{ is integer.}$$

Causality and physical realisation — Paley Wiener Criteria :-

It is a test which distinguish the physical realisable char. from unrealisable one.

Condition for Causality and physical realisation in

t-domain :-

"Condition for physically realisable system is that it must ^{be} causal system."

An LTI system is causal iff $h(t) = 0$ for $t < 0$.

So, the necessary & sufficient condition for physically realisable system is their impulse response $h(t)$ is zero for $t < 0$.

Condition for causality and physical realisation in
f-domain :-

Paley Wiener criteria, implies that the necessary and sufficient condition for the magnitude system funct. $H(\omega)$ to be physically

realisable is satisfies the following condition:-

$$\int_{-\infty}^{\infty} \frac{\ln |H(\omega)|}{1+\omega^2} d\omega < \infty \quad - \text{ Paley Wiener criteria.}$$

It is physically realisable, however the magnitude square of transfer function of system is absolutely integrable before Paley-Wiener criteria valid.

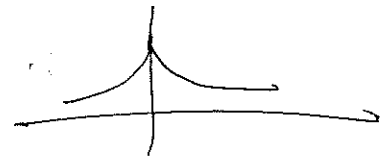
i.e; $\int_{-\infty}^{\infty} |H(\omega)|^2 d\omega < \infty.$

Conclusions:

Significant conclusions drawn from Paley-Wiener criteria : —

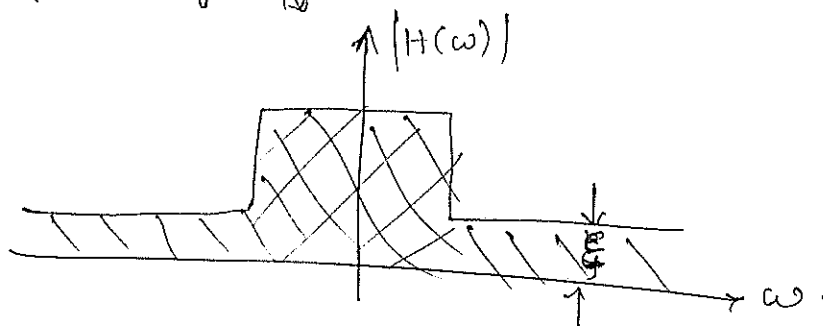
- (i) The transfer fn.'s of the system is zero at some discrete instants of frequencies but it cannot be zero over ~~with~~ ^{within} the band of frequencies ~~of~~.
- (ii) The transfer function magnitude function is not fall off to zero.

Thus $|H(\omega)| = k e^{-\alpha|\omega|}$



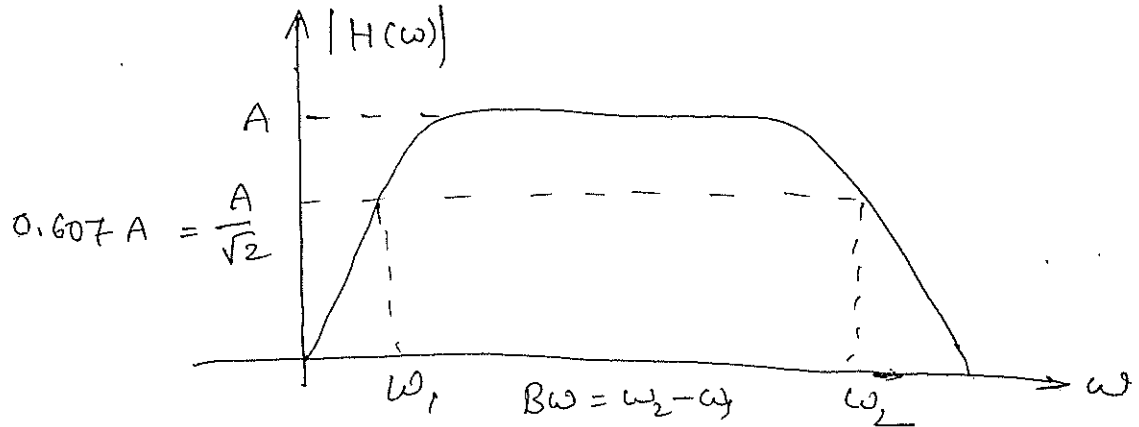
It is permissible.

- (iii) The system transfer fn. magnitude fn.'s have not high attenuation factor.
- (iv) The characteristics of physically realisable low-pass filter which is permissible for small values of ϵ as shown in figure.



SYSTEM BAND WIDTH:-

Def:- The System bandwidth is arbitrarily defined as the band of frequency over which the magnitude $|H(\omega)|$ is $\frac{1}{\sqrt{2}}$ times its mid band value.



i.e., Bandwidth = $(\omega_2 - \omega_1)$ as shown in Fig.

* Find the convolution b/w the following signals discrete
 $u(n) = x(n)$; $h(n) = u(n)$.

$$\begin{aligned} \rightarrow y(n) &= x(n) * h(n) = \sum_{k=-\infty}^{\infty} x(k) h(n-k) \\ &= \sum_{k=-\infty}^{\infty} u(k) \cdot u(n-k) \end{aligned}$$

$$u(k) = \begin{cases} 1 & \text{for } k \geq 0 \\ 0 & \text{for } k < 0 \end{cases}$$

$$= \sum_{k=0}^{\infty} 1 \cdot u(n-k)$$

$$u(n-k) = \begin{cases} 1 & \text{for } n-k \geq 0 \\ & k \leq n \\ 0 & \text{for } k > n. \end{cases} = \sum_{k=0}^n 1 \cdot 1 = \sum_{k=0}^n 1$$

$$= n - 0 + 1$$

$$= \underline{\underline{n+1}}$$

$$\therefore y(n) = \underline{\underline{n+1}}$$

$$* \quad x(n) = 2^n u(n); \quad h(n) = \frac{1}{2^n} u(n)$$

$$\begin{aligned} \rightarrow y(n) &= x(n) * h(n) = \sum_{k=-\infty}^{\infty} x(k) h(n-k) \\ &= \sum_{k=-\infty}^{\infty} 2^k u(k) \cdot \frac{1}{2^{n-k}} u(n-k) \\ &= \sum_{k=0}^{n+k} 1 \cdot u(n-k) \\ &= 2^{2k-n} \sum_{k=0}^n 1 \\ &= \sum_{k=0}^n 2^{2k-n} \\ &= \sum_{k=0}^n \frac{2^{2k}}{2^n} \\ &= \frac{1}{2^n} \cdot \sum_{k=0}^n 2^{2k} = \frac{1}{2^n} \sum_{k=0}^n 4^k \\ &= \frac{1}{2^n} \cdot \frac{4^{n+1} - 1}{4 - 1} \\ &= \frac{4^{n+1} - 1}{3 \times 2^n} \end{aligned}$$

$$* \quad x(n) = \delta(n); \quad h(n) = u(n).$$

$$\begin{aligned} \rightarrow y(n) &= x(n) * h(n) = \sum_{k=-\infty}^{\infty} \delta(k) u(n-k) \\ &= \sum_{k=-\infty}^{\infty} \delta(k) u(n-k) \end{aligned}$$

$$\therefore \delta(n) = \begin{cases} 1 \\ 0 \end{cases}$$

$n=0 \Rightarrow$
otherwise \Rightarrow

$$\sum_{k=0}^{\infty} u(n-k)$$

$$= \underline{\underline{u(n)}}$$

Frequency Integration property :-

$$\text{If } g(t) \longleftrightarrow G(\omega), \text{ then } \frac{g(t)}{-jt} \longleftrightarrow \int G(\omega) d\omega.$$

Pf:- $g(t) \longleftrightarrow G(\omega).$

Applying integration on both sides w.r.t 'd ω '

$$\Rightarrow \int g(t) d\omega \longleftrightarrow \int G(\omega) d\omega.$$

$$\Rightarrow G(\omega) = \int_{-\infty}^{\infty} g(t) e^{-j\omega t} dt$$

$$\int G(\omega) d\omega = \int_{-\infty}^{\infty} g(t) \int e^{-j\omega t} d\omega dt$$

$$= \int_{-\infty}^{\infty} g(t) \frac{e^{-j\omega t}}{-j\omega t} dt$$

$$= \int_{-\infty}^{\infty} \frac{g(t)}{-jt} e^{-j\omega t} dt$$

$$= F\left[\frac{g(t)}{-jt}\right]$$

∴

$$\boxed{\frac{g(t)}{-jt} \longleftrightarrow \int G(\omega) d\omega.}$$

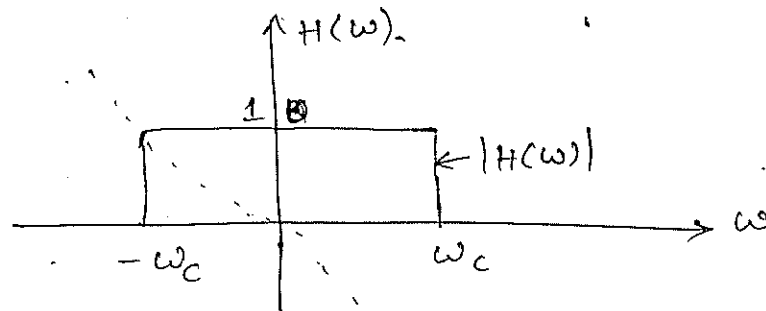
17/8/06 Ideal Filters :-

There are 3 types of ideal filters.

1. Ideal low pass filter.
2. Ideal high pass filter.
3. Ideal band pass filter.

1. Ideal low pass filter :-

The spectral characteristics of ideal low pass filter are as shown in figure.



$$H(\omega) = |H(\omega)| e^{j\angle H(\omega)}$$

$$|H(\omega)| = \begin{cases} 1 & \text{for } -\omega_c \leq \omega \leq \omega_c \\ 0 & \text{elsewhere.} \end{cases}$$

$$H(\omega) = \begin{cases} 1 e^{-j\omega t_0} & \text{for } -\omega_c \leq \omega \leq \omega_c \\ 0 e^{-j\omega t_0} = 0 & \text{elsewhere.} \end{cases}$$

Impulse response calculation $h(t)$:-

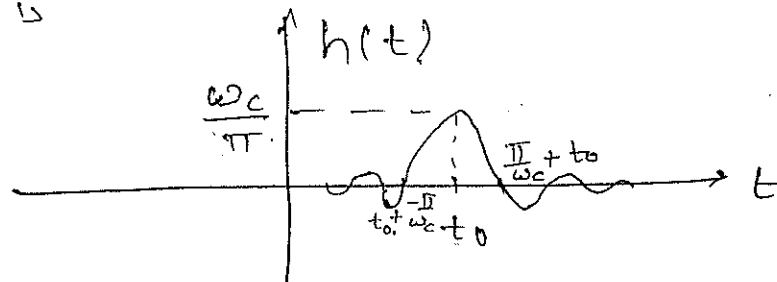
$$\mathcal{F}^{-1} [H(\omega)] = h(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} H(\omega) e^{j\omega t} d\omega$$

$$h(t) = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{-j\omega t_0} e^{j\omega t} d\omega.$$

$$= \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{j\omega(t-t_0)} d\omega$$

$$\begin{aligned}
 &= \frac{j}{2\pi} \cdot \frac{e^{j\omega(t-t_0)}}{j(t-t_0)} \Big|_{-\omega_c}^{\omega_c} \\
 &= \frac{1}{\pi(t-t_0)} \left[\frac{e^{j\omega_c(t-t_0)} - e^{-j\omega_c(t-t_0)}}{2j} \right] \\
 &= \frac{1}{\pi(t-t_0)} \sin[\omega_c(t-t_0)] \\
 &= \frac{\omega_c}{\pi} \times \frac{\sin[\omega_c(t-t_0)]}{\omega_c(t-t_0)} \\
 &= \frac{\omega_c}{\pi} \cdot \text{sinc}[\omega_c(t-t_0)]
 \end{aligned}$$

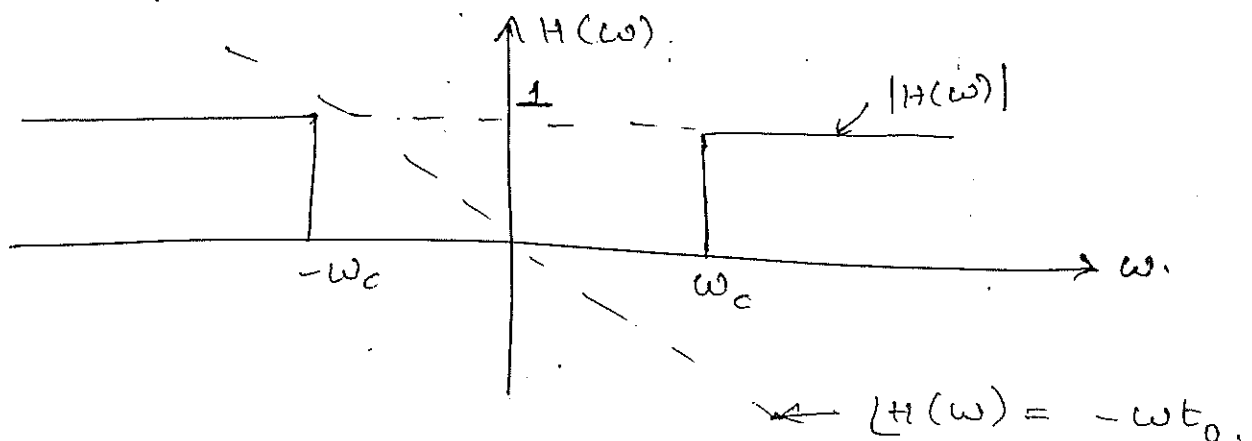
Generalised
 $h(t)$ spectrum is



From this, the impulse response exist for -ve value of time i.e; $h(t) \neq 0$ for $t < 0$. So, the system is non-Causal system. Hence it is not physically realisable.

2. Ideal high pass filter:-

The spectral char. of ideal high pass filter is



$$|H(\omega)| = \begin{cases} 1 & \text{for } \omega_c \leq \omega \leq \omega_b \text{ and } -\omega_b \leq \omega \leq -\omega_c \\ 0 & \text{elsewhere i.e. } -\omega_c \leq \omega \leq \omega_c \end{cases}$$

$$\angle H(\omega) = -\omega t_0$$

$$H(\omega) = \begin{cases} 1 \times e^{-j\omega t_0} & ; \omega_c \leq \omega \leq \omega_b \text{ and } -\omega_b \leq \omega \leq -\omega_c \\ 0 & ; -\omega_c \leq \omega \leq \omega_c \end{cases}$$

Impulse response calculation, $F^{-1}[H(\omega)] = h(t)$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} H(\omega) e^{j\omega t} d\omega$$

$$h(t) = \frac{1}{2\pi} \left[\int_{-\omega_b}^{-\omega_c} e^{-j\omega t_0} e^{j\omega t} d\omega + 0 + \int_{\omega_c}^{\omega_b} e^{-j\omega t_0} e^{j\omega t} d\omega \right]$$

$$= \frac{1}{2\pi} \left[\frac{e^{j\omega(t-t_0)}}{j(t-t_0)} \Big|_{-\omega_b}^{-\omega_c} + \frac{e^{j\omega(t-t_0)}}{j(t-t_0)} \Big|_{\omega_c}^{\omega_b} \right]$$

$$= \frac{1}{2\pi} \left[\frac{e^{-j\omega_c(t-t_0)}}{j(t-t_0)} - \frac{e^{j\omega_c(t-t_0)}}{j(t-t_0)} \right]$$

$$= \frac{-1}{\pi(t-t_0)} \left[\frac{e^{j\omega_c(t-t_0)} - e^{-j\omega_c(t-t_0)}}{2j} \right]$$

$$= \frac{-1}{\pi(t-t_0)} \sin[\omega_c(t-t_0)]$$

$$= \frac{-\omega_c}{\pi} \text{Sinc}[\omega_c(t-t_0)]$$

\therefore It cannot be physically realisable. Impulse values cannot exist for -ve values of time.

(or) Alternative method :-

From the spectrum,

$$H(\omega) = e^{-j\omega t_0} u(-\omega - \omega_c) + e^{-j\omega t_0} u(\omega - \omega_c)$$

we know that

$$g(t) \longleftrightarrow G(\omega)$$

$$u(t) \longleftrightarrow \frac{1}{j\omega} + \pi \delta(\omega)$$

$$G(\omega) \longleftrightarrow 2\pi g(-\omega)$$

$$\frac{1}{j\omega} + \pi \delta(\omega) \longleftrightarrow 2\pi u(-\omega)$$

$$\left(\frac{1}{j\omega} + \pi \delta(\omega) \right) e^{-j\omega_c t} \longleftrightarrow 2\pi u(-\omega - \omega_c)$$

$$\left(\frac{1}{j(t-t_0)} + \pi \delta(t-t_0) \right) e^{-j\omega_c(t-t_0)} \longleftrightarrow 2\pi e^{-j\omega t_0} u(-\omega - \omega_c)$$

$$g(-t) \longleftrightarrow G(-\omega)$$

$$\frac{1}{-jt} + \pi \delta(-t) \longleftrightarrow 2\pi u(-(-\omega))$$

$$\frac{1}{-jt} + \pi \delta(t) \longleftrightarrow 2\pi u(\omega) \quad \left(\begin{array}{l} \because \delta(t) \text{ satisfies} \\ \text{even sym.} \end{array} \right)$$

$$\left(\frac{1}{-jt} + \pi \delta(t) \right) e^{j\omega_c t} \longleftrightarrow 2\pi u(\omega - \omega_c)$$

$$\left(\frac{1}{-j(t-t_0)} + \pi \delta(t-t_0) \right) e^{j\omega_c(t-t_0)} \longleftrightarrow 2\pi e^{-j\omega t_0} u(\omega - \omega_c)$$

$$F^{-1}[H(\omega)] = F^{-1}\left[e^{-j\omega t_0} u(-\omega - \omega_c) \right] + F^{-1}\left[e^{-j\omega t_0} u(\omega - \omega_c) \right]$$

$$= \frac{1}{2\pi} \left(\frac{1}{j(t-t_0)} + \pi \delta(t-t_0) \right) e^{-j\omega_c(t-t_0)} + \frac{1}{2\pi} \left(\frac{1}{-j(t-t_0)} + \pi \delta(t-t_0) \right) e^{j\omega_c(t-t_0)}$$

$$\Rightarrow h(t) = \frac{1}{2\pi} \pi \delta(t-t_0) \left[\frac{e^{j\omega_c(t-t_0)} + e^{-j\omega_c(t-t_0)}}{2} \right] + \frac{1}{2\pi} \pi \delta(t-t_0) \left[\frac{e^{j\omega_c(t-t_0)} - e^{-j\omega_c(t-t_0)}}{2j} \right]$$

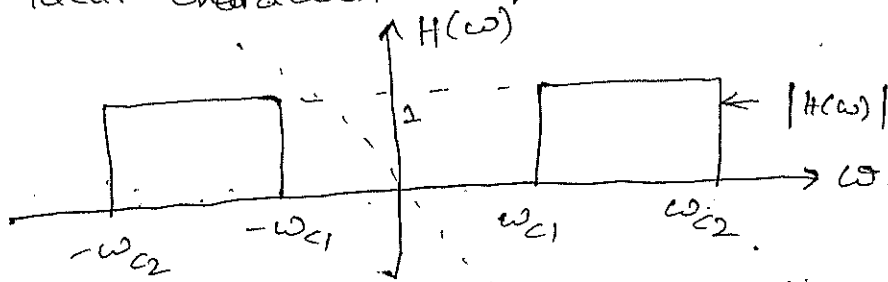
$$= \delta(t-t_0) \cos[\omega_c(t-t_0)] - \frac{1}{\pi(t-t_0)} \sin[\omega_c(t-t_0)]$$

$$h(t) = \delta(t-t_0) - \frac{\omega_c}{\pi} \text{Sinc}[\omega_c(t-t_0)]$$

This is not physically realisable. (∵ At $t=t_0$, $\cos \omega_c(t-t_0) = 0$)

(iii) Ideal Band pass filter :-

The ideal characteristics of ideal band pass filter is:



$$\rightarrow [H(\omega) = -\omega t_0]$$

$$H(\omega) = \begin{cases} 1 \times e^{-j\omega t_0} & ; -\omega_{c2} \leq \omega \leq -\omega_{c1} ; \omega_{c1} \leq \omega \leq \omega_{c2} \\ 0 & ; \text{else where} \end{cases}$$

Impulse response is

$$F^{-1}[H(\omega)] = h(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} H(\omega) e^{j\omega t} d\omega$$

$$h(t) = \frac{1}{2\pi} \left[\int_{-\omega_{c2}}^{-\omega_{c1}} e^{-j\omega t_0} e^{j\omega t} d\omega + \int_{\omega_{c1}}^{\omega_{c2}} e^{-j\omega t_0} e^{j\omega t} d\omega \right]$$

$$= \frac{1}{2\pi} \left[\frac{e^{j\omega(t-t_0)}}{j(t-t_0)} \Big|_{-\omega_{c2}}^{-\omega_{c1}} + \frac{e^{j\omega(t-t_0)}}{j(t-t_0)} \Big|_{\omega_{c1}}^{\omega_{c2}} \right]$$

$$= \frac{1}{2\pi} \left[\frac{e^{-j\omega_1(t-t_0)} - e^{-j\omega_2(t-t_0)}}{j(t-t_0)} + \frac{e^{j\omega_2(t-t_0)} - e^{j\omega_1(t-t_0)}}{j(t-t_0)} \right]$$

$$= \frac{1}{2\pi} \left[\frac{e^{j\omega_2(t-t_0)} - e^{-j\omega_2(t-t_0)}}{2j} - \left[\frac{e^{j\omega_1(t-t_0)} - e^{-j\omega_1(t-t_0)}}{2j} \right] \right]$$

$$= \frac{1}{\pi(t-t_0)} \left[\sin(\omega_2(t-t_0)) - \sin(\omega_1(t-t_0)) \right]$$

$$\therefore h(t) = \frac{\omega_c}{\pi} \left[\text{sinc}(\omega_2(t-t_0)) - \text{sinc}(\omega_1(t-t_0)) \right]$$

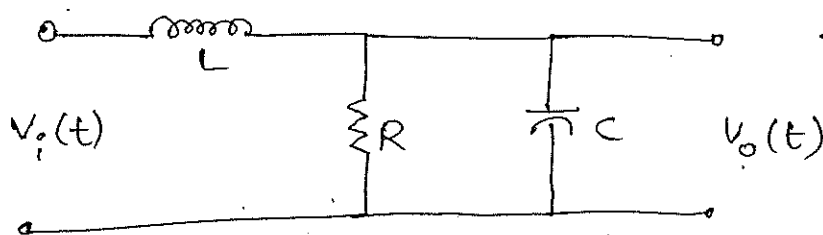
$h(t)$ exist for -ve values of time. Hence

$h(t) \neq 0$ for $t < 0$. So it is not physically realisable.

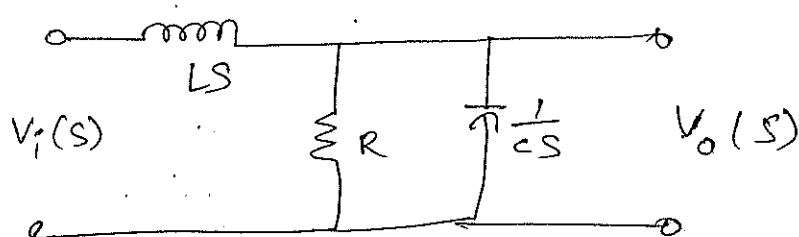
Example for practical low pass (or) physically realisable

low pass filter :-

The practical RLC - low pass ckt is as shown in figure.



Eq. Laplace S-domain ckt is



$$V_o(s) = \left(R \parallel \frac{1}{Cs} \right) I(s) = \frac{R \cdot \frac{1}{Cs}}{R + \frac{1}{Cs}} \cdot I(s)$$

$$= \frac{R}{1 + sCR} I(s)$$

$$V_i(s) = \left[LS + \left(R \parallel \frac{1}{Cs} \right) \right] I(s)$$

$$= \left[LS + \frac{R}{1 + sCR} \right] I(s)$$

$$= \frac{LS(1 + sCR) + R}{1 + sCR} I(s)$$

$$\frac{V_o(s)}{V_i(s)} = \frac{R / (1 + sCR)}{LS(1 + sCR) + R / (1 + sCR)} = \frac{R}{LS(1 + sCR) + R}$$

$$\Rightarrow \frac{V_o(s)}{V_i(s)} = H(s) = \frac{R}{s^2 LCR + LS + R}$$

$$\Rightarrow H(s) = \frac{1}{s^2 LC + s \cdot \frac{L}{R} + 1}$$

$$H(s) = H(j\omega) = \frac{1}{-\omega^2 LC + j\omega \frac{L}{R} + 1} \quad (\because s = j\omega)$$

$$H(j\omega) = \frac{1}{LC} \left[\frac{1}{-\omega^2 + j\omega \cdot \frac{1}{RC} + \frac{1}{LC}} \right]$$

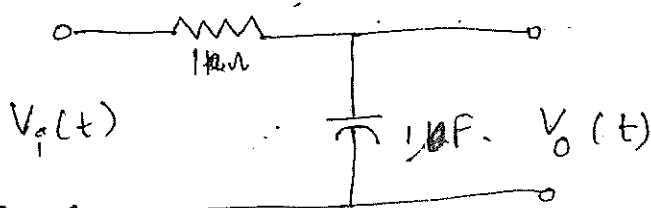
$$H(s) = \frac{1}{LC} \left[\frac{1}{s^2 + s \cdot \frac{1}{RC} + \frac{1}{LC}} \right]$$

$$= \frac{1}{LC} \left[\frac{1}{s^2 + 2s \cdot \frac{1}{2RC} + \frac{1}{LC} + \left(\frac{1}{2RC} \right)^2 - \left(\frac{1}{2RC} \right)^2} \right]$$

$$= \frac{1}{LC} \left[\frac{1}{\left(s + \frac{1}{2RC} \right)^2 + \frac{1}{LC} - \left(\frac{1}{2RC} \right)^2} \right]$$

$$= \frac{1}{LC} \left[\frac{1}{\left(s + \frac{1}{2RC}\right)^2} - \left(\frac{-1}{LC} + \left(\frac{1}{2RC}\right)^2 \right) \right]$$

* The practical, low pass filter is as shown in the figure. Find the o/p power spectral density, o/p power, mean square value and RMS value of o/p signal.

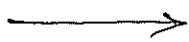


Given I/P Spectral densities are

(a) $S_i(\omega) = K$

(b) $S_i(\omega) = G_2(\omega)$ (i.e. gate fn. width is ' ω ')

(c) $S_i(\omega) = \pi [\delta(\omega - 1) + \delta(\omega + 1)]$



Relation b/w i/p & o/p spectral densities :-

We know that I/P & O/P relation of LTI system

is $y(t) = x(t) * h(t)$

$$F[y(t)] = F[x(t) * h(t)]$$

$$\Rightarrow Y(\omega) = X(\omega) \cdot H(\omega), \text{ where}$$

$X(\omega)$ is I/P ^{signal} spectrum.

$Y(\omega)$ is o/p signal spectrum.

$H(\omega)$ is transfer fn. of the system (or) freq. response.

Applying both sides absolute value,

$$\begin{aligned} |Y(\omega)| &= |X(\omega)| \cdot |H(\omega)| \\ &= |H(\omega)| \cdot |X(\omega)| \end{aligned}$$

Applying square on both sides

$$|Y(\omega)|^2 = |H(\omega)|^2 \cdot |X(\omega)|^2$$

Energy Spectral density of $g(t)$ is -

$$\Psi_g(\omega) = |G(\omega)|^2 \quad (\text{J/Hz})$$

Energy spectral density of I/P signal is

$$\Psi_x(\omega) = S_i(\omega) = |X(\omega)|^2$$

Energy spectral density of O/P is

$$\Psi_y(\omega) = S_o(\omega) = |Y(\omega)|^2$$

(or)

$$S_o(\omega) = |H(\omega)|^2 S_i(\omega)$$

(a)

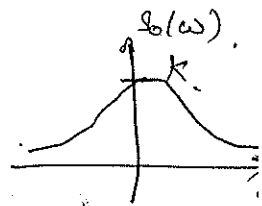
$$H(\omega) = \frac{\frac{V_o(s)}{V_i(s)}}{1 + \frac{1}{j\omega}} = \frac{1}{1 + j\omega}$$

$$|H(\omega)| = \frac{1}{\sqrt{1+\omega^2}} \Rightarrow |H(\omega)|^2 = \frac{1}{1+\omega^2}$$

Output Spectral density is

$$S_o(\omega) = \Psi_y(\omega) = |H(\omega)|^2 S_i(\omega)$$

$$S_o(\omega) = \frac{1}{1+\omega^2} \times K = \frac{K}{1+\omega^2} \text{ Watt/Hz}$$



$$\text{Power} = \frac{1}{2\pi} \int_{-\infty}^{\infty} S_o(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{K}{1+\omega^2} d\omega = \frac{K}{2\pi} \cdot \tan^{-1}(\omega) \Big|_{-\infty}^{\infty}$$

$$= \frac{K}{2\pi} \left(\frac{\pi}{2} + \frac{\pi}{2} \right)$$

$$= \frac{K}{2} \text{ Watts}$$

Mean Square Value :-

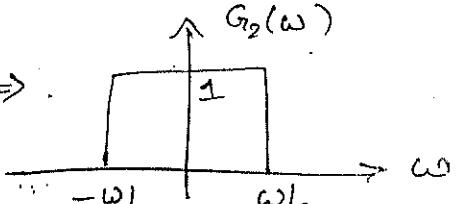
O/p signal power is nothing but the mean square value of o/p signal.

Mean Square value is $\frac{1}{T} \int_{-T}^T |g(t)|^2 dt$, watts

This is nothing but power. $\left(\frac{1}{2\pi} \int_{-\infty}^{\infty} S_o(\omega) d\omega \right)$

Root of mean square value is rms value.

\therefore RMS value = $\sqrt{\frac{P}{2}}$ //

(b) $S_i(\omega) = G_2(\omega) \Rightarrow$ 

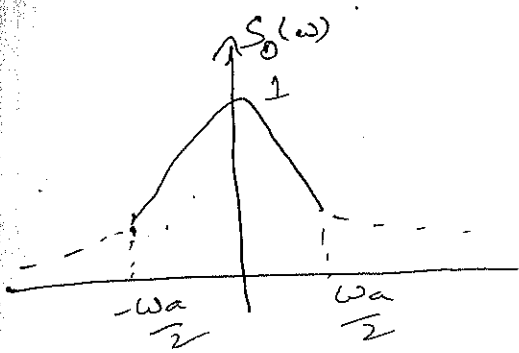
$H(\omega) = \frac{1}{1+j\omega} ; |H(\omega)|^2 = \frac{1}{1+\omega^2}$

O/p Spectral density is...

$S_o(\omega) = |H(\omega)|^2 S_i(\omega)$

$= \frac{1}{1+\omega^2} \cdot |G_2(\omega)|^2$

$= \begin{cases} \frac{1}{1+\omega^2} \times 1^2 ; & -\frac{\omega_a}{2} \leq \omega \leq \frac{\omega_a}{2} \\ 0 & \text{else..} \end{cases}$



Power, $P = \frac{1}{2\pi} \int_{-\frac{\omega_a}{2}}^{\frac{\omega_a}{2}} \frac{1}{1+\omega^2} d\omega = \frac{1}{2\pi} \tan^{-1}(\omega) \Big|_{-\frac{\omega_a}{2}}^{\frac{\omega_a}{2}}$
 $= \frac{1}{\pi} \tan^{-1}\left(\frac{\omega_a}{2}\right)$

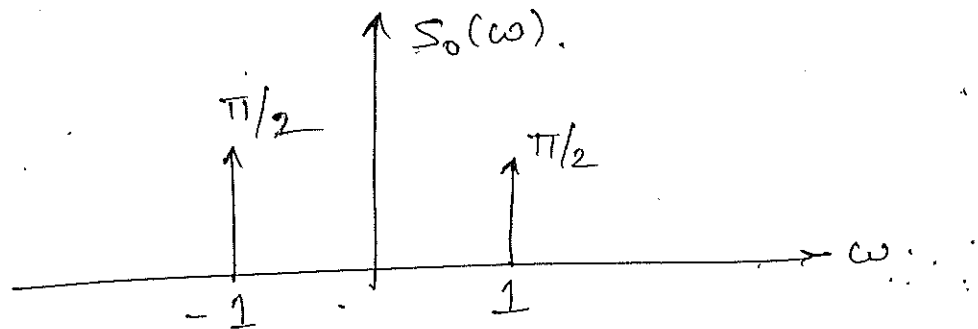
Mean Square = Power.

RMS = $\sqrt{\text{Power}} = \sqrt{\frac{1}{\pi} \tan^{-1}\left(\frac{\omega_a}{2}\right)}$

$$\textcircled{c} \quad S_i(\omega) = \pi [\delta(\omega-1) + \delta(\omega+1)]$$

$$S_o(\omega) = \frac{1}{1+\omega^2} \cdot \pi [\delta(\omega-1) + \delta(\omega+1)]$$

$$= \frac{\pi}{1+\omega^2} \delta(\omega-1) + \frac{\pi}{1+\omega^2} \delta(\omega+1)$$



(a)

$$\text{Power} = \frac{1}{2\pi} \left[\int_{-\infty}^{\infty} \frac{\pi}{1+\omega^2} \delta(\omega-1) d\omega + \int_{-\infty}^{\infty} \frac{\pi}{1+\omega^2} \delta(\omega+1) d\omega \right]$$

$$= \frac{1}{2\pi} \left(\frac{\pi}{1+1^2} + \frac{\pi}{1+(-1)^2} \right)$$

$$= \frac{1}{2\pi} (\pi) = \frac{1}{2} //$$

$$\text{Mean Square Value} = \text{power} = \frac{1}{2}$$

$$\text{RMS value} = \sqrt{\text{Power}} = \frac{1}{\sqrt{2}} //$$